

JFET Input Operational Amplifiers

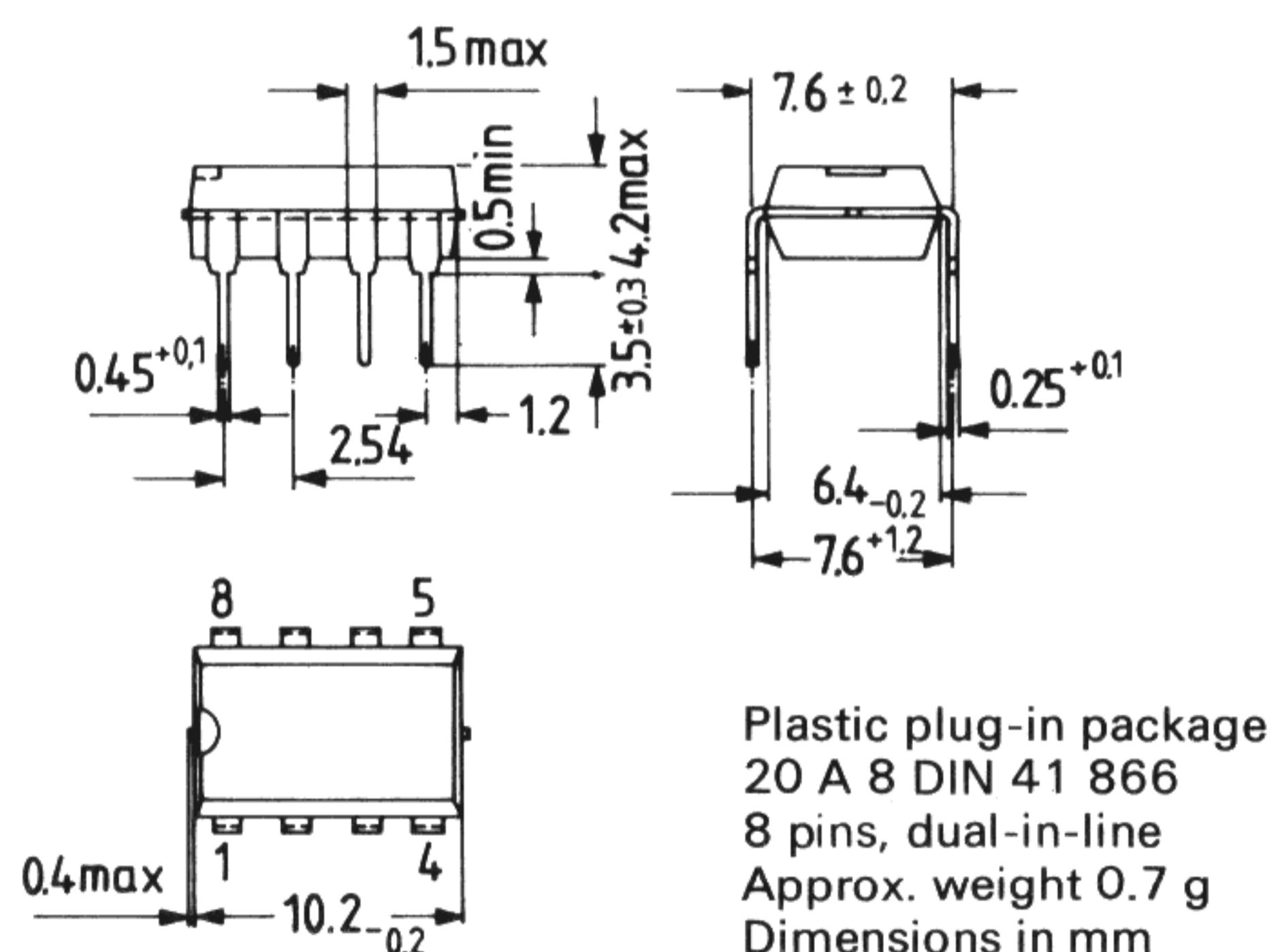
LF 355 N
LF 356 N
LF 357 N

These operational amplifiers have JFET input transistors and are outstanding for very low input and offset currents. The output is designed for high capacitive load without any stability problems.

Further features:

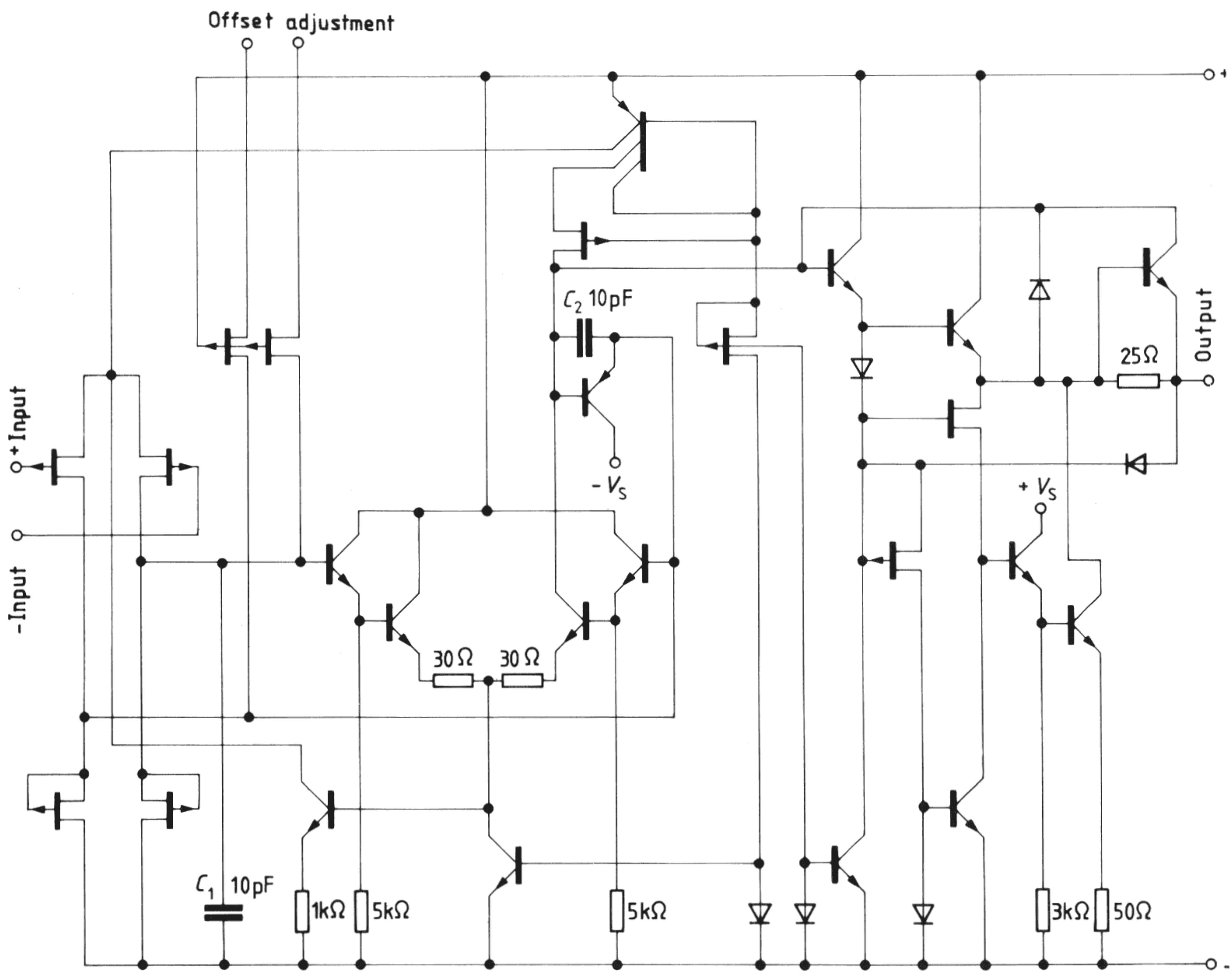
- Extremely high input resistance
- Slight drifting at temperature changes
- Wide bandwidth
- High input voltage up to $+V_S$ permitted
- Internal frequency compensation

Type	Ordering code
LF 355 N	Q67000-A1397
LF 356 N	Q67000-A1404
LF 357 N	Q67000-A1399

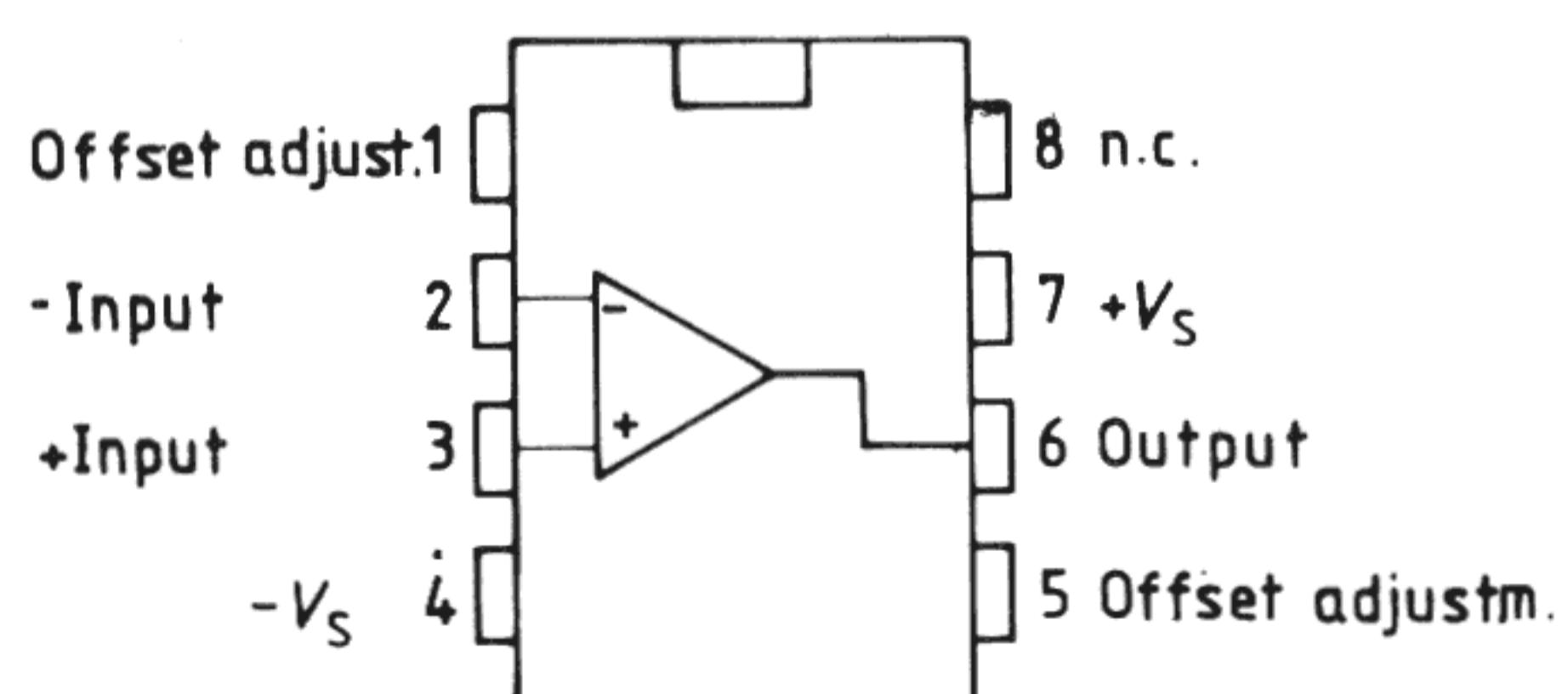


Plastic plug-in package
20 A 8 DIN 41 866
8 pins, dual-in-line
Approx. weight 0.7 g
Dimensions in mm

Circuit diagram



Pin configuration



Maximum ratings

Supply voltage	V_S	± 18	V
Differential input voltage	V_{ID}	± 30	V
Output short-circuit duration	t_{QSC}	∞	
Storage temperature range	T_s	-55 to +125	°C
Junction temperature	T_j	100	°C
Thermal resistance system – ambient air	R_{thsamb}	175	K/W

Range of operation

Supply voltage	V_S	± 5 to ± 18	V
Input voltage	V_I	± 16	V
$-V_S = 18$ to 16 V; $+V_S = 5$ to 16 V	V_I	$-V_S$ to 16	V
$-V_S = 5$ to 16 V; $+V_S = 5$ to 16 V	T_{amb}	0 to +70	°C
Ambient temperature			

Electrical characteristics $V_S = \pm 15$ V, $T_{amb} = 25$ °C

			min	typ	max	
Supply current	LF 355 N	I_S	2	4	mA	
	LF 356 N, LF 357 N	I_S	5	10	mA	
Input offset voltage	($R_G = 50$ Ω)	V_{IO}	3	10	mV	
Input offset current		I_{IO}	3	50	pA	
Input current		I_I	30	200	pA	
Input resistance		R_I	10^{12}		Ω	
Open-loop voltage amplification		A_{VO}	80	106	dB	
Rate of voltage rise	LF 355 N: $A_V = 1$ LF 356 N: $A_V = 1$ LF 357 N: $A_V = 5$	$\frac{dvq}{dtr}$	5 12 50		V/μs	
Performance bandwidth	LF 355 N LF 356 N LF 357 N	f_p	2.5 5 20		MHz	
Transient time (for 0.01%)	LF 355 N LF 356 N, LF 357 N	t_r	4 1.5		μs	
Input noise voltage						
$R_S = 100$ Ω; $f = 100$ Hz:	LF 355 N	V_{IN}	25		nV/√Hz	
	LF 356 N, LF 357 N	V_{IN}	15		nV/√Hz	
$R_S = 100$ Ω, $f = 1000$ Hz:	LF 355 N	V_{IN}	20		nV/√Hz	
	LF 356 N, LF 357 N	V_{IN}	12		nV/√Hz	
Input noise current						
$f = 100$ Hz, or 1000 Hz		I_{IN}	0.01		pA/√Hz	
Input capacitance		C_I	3		pF	

Characteristics

$V_S = \pm 15 \text{ V}$; $T_{\text{amb}} = 0 \text{ to } +70^\circ\text{C}$,
unless otherwise specified

Input offset voltage $R_G = 50 \Omega$

Temperature coefficient of V_{IO} : $R_S = 50 \Omega$

Change of α_{VIO}

after a change of V_{IO} adjustment¹⁾

Input offset current $T_j = 70^\circ\text{C}$

Input current²⁾ $T_j = 70^\circ\text{C}$

Open-loop voltage amplification

$R_L = 2 \text{ k}\Omega$, $V_{Qpp} = \pm 10 \text{ V}$

Output voltage $R_L = 10 \text{ k}\Omega$

$R_L = 2 \text{ k}\Omega$

Input common mode range

Common mode rejection

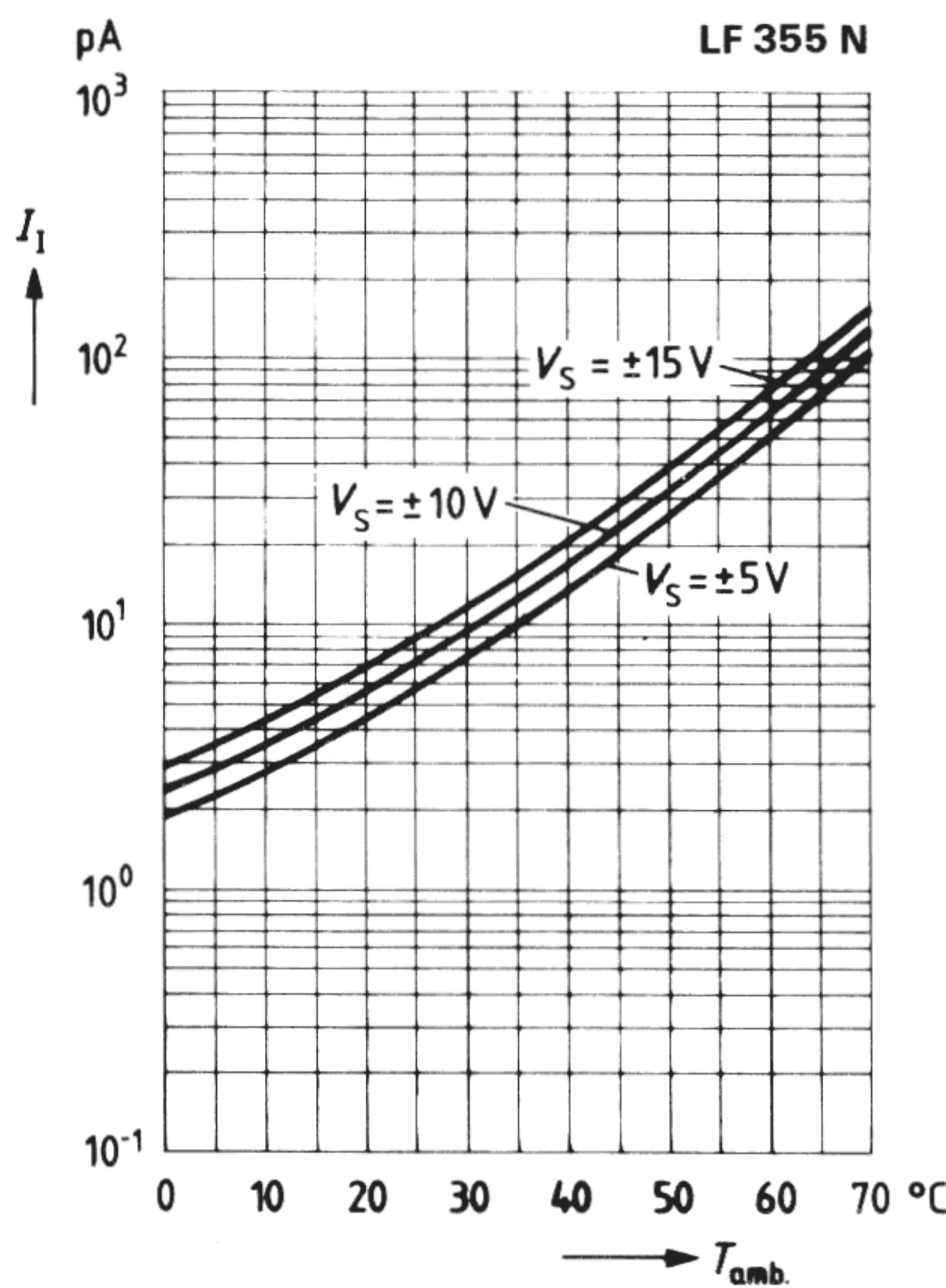
Supply voltage rejection

	min	typ	max	
V_{IO}			14	mV
α_{VIO}	5			$\mu\text{V/K}$
$\Delta \alpha_{\text{VIO}}$	0.5			per mV
I_{IO}			2	nA
I_I		8		nA
A_{VO}	63			dB
V_{Qpp}	12	± 13	-12	V
V_{Qpp}	10	± 12	-10	V
V_{IC}	± 11	-12		V
k_{CMR}	80	100		dB
k_{SVR}	80	100		dB

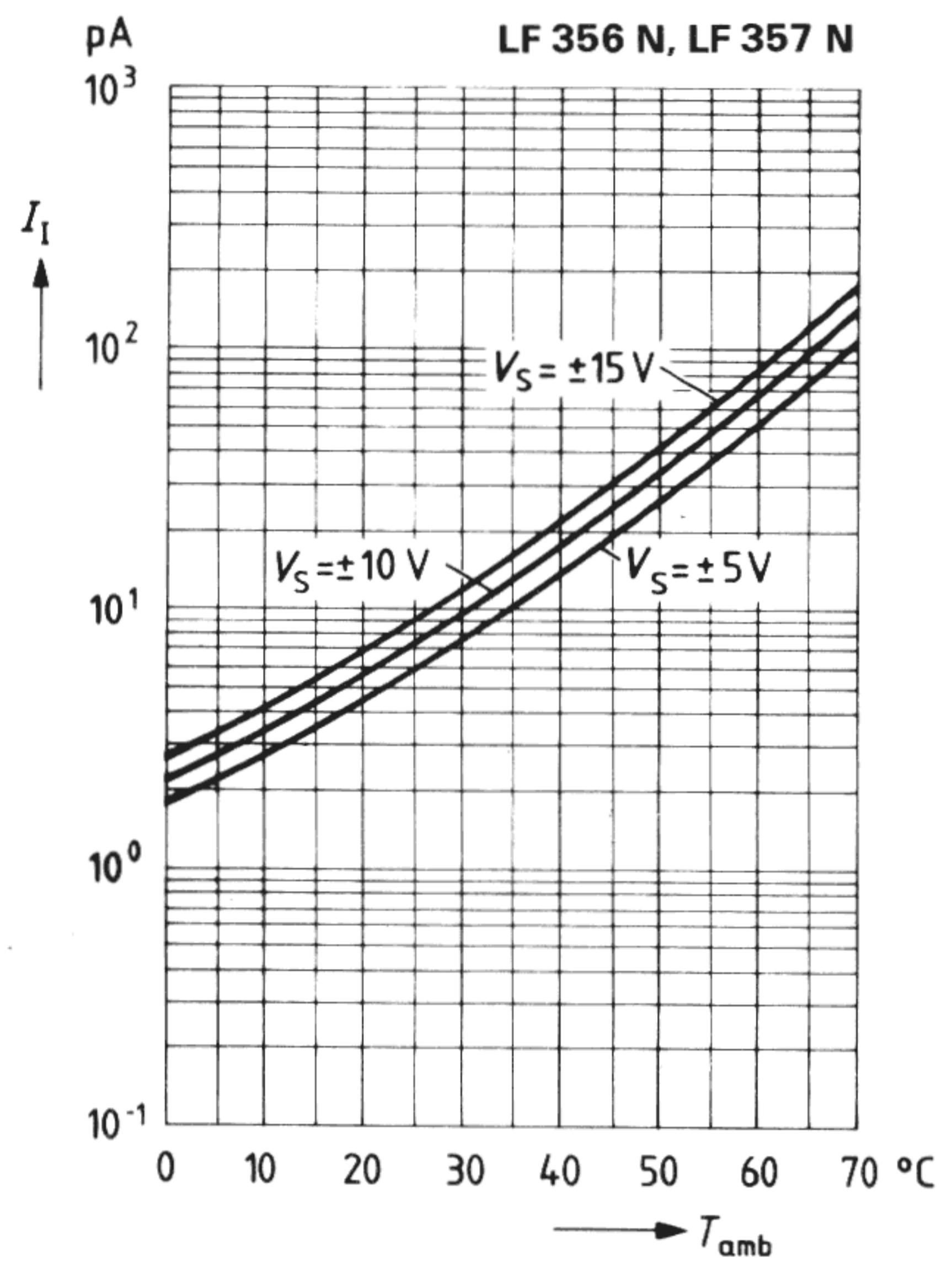
Remarks:

- 1) Compared to the originally non-adjusted value, the temperature coefficient of the adjusted input offset voltage only slightly changes (typ. 0.5 $\mu\text{V/K}$) for every mV of the setting range. Adjusting the offset voltage is of no effect on the common-mode rejection and open-loop voltage amplification.
- 2) The input currents become approximately twice as great with every 10 K increase in junction temperature.

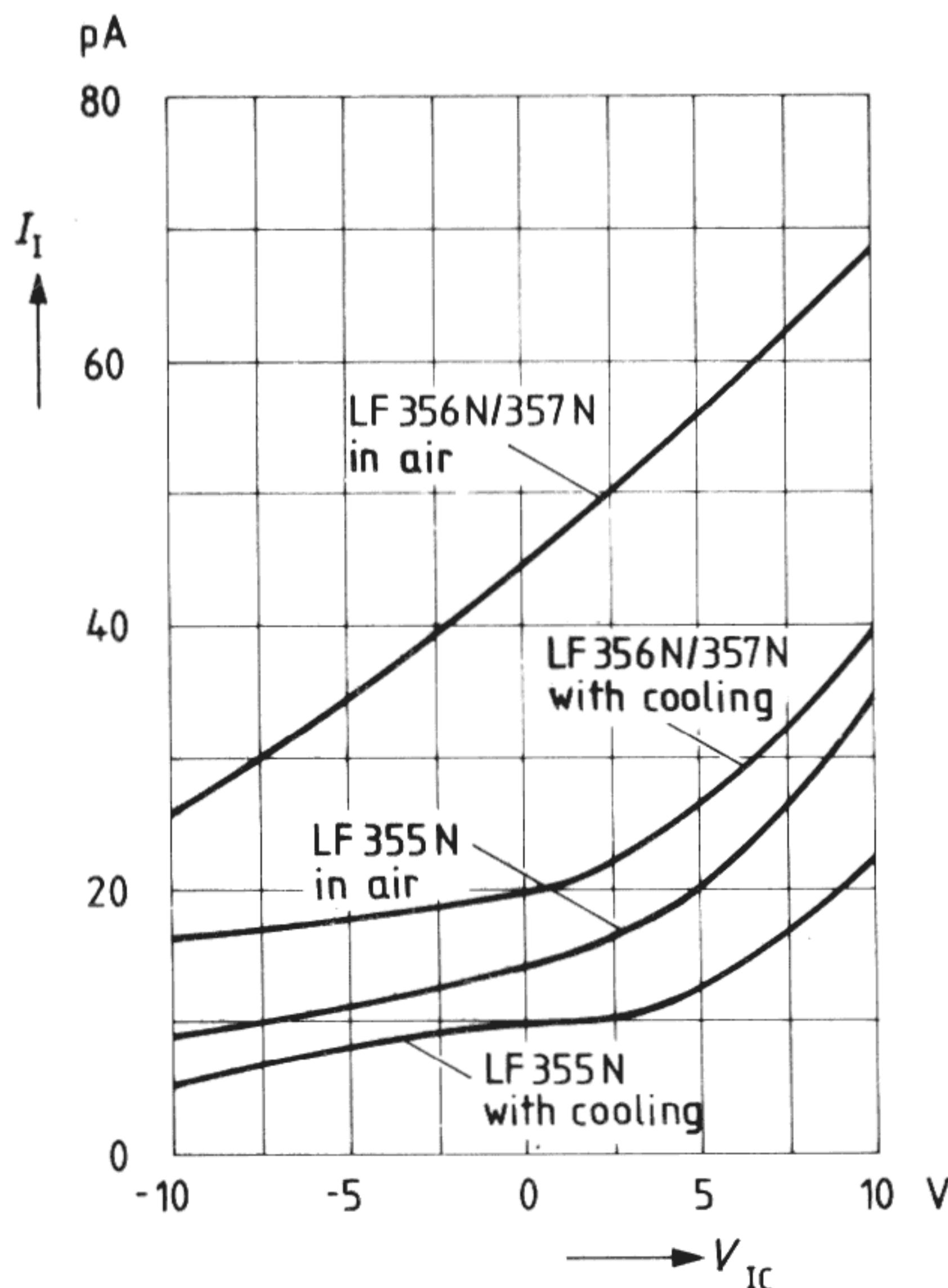
Input current $I_I = f(T_{\text{amb}})$



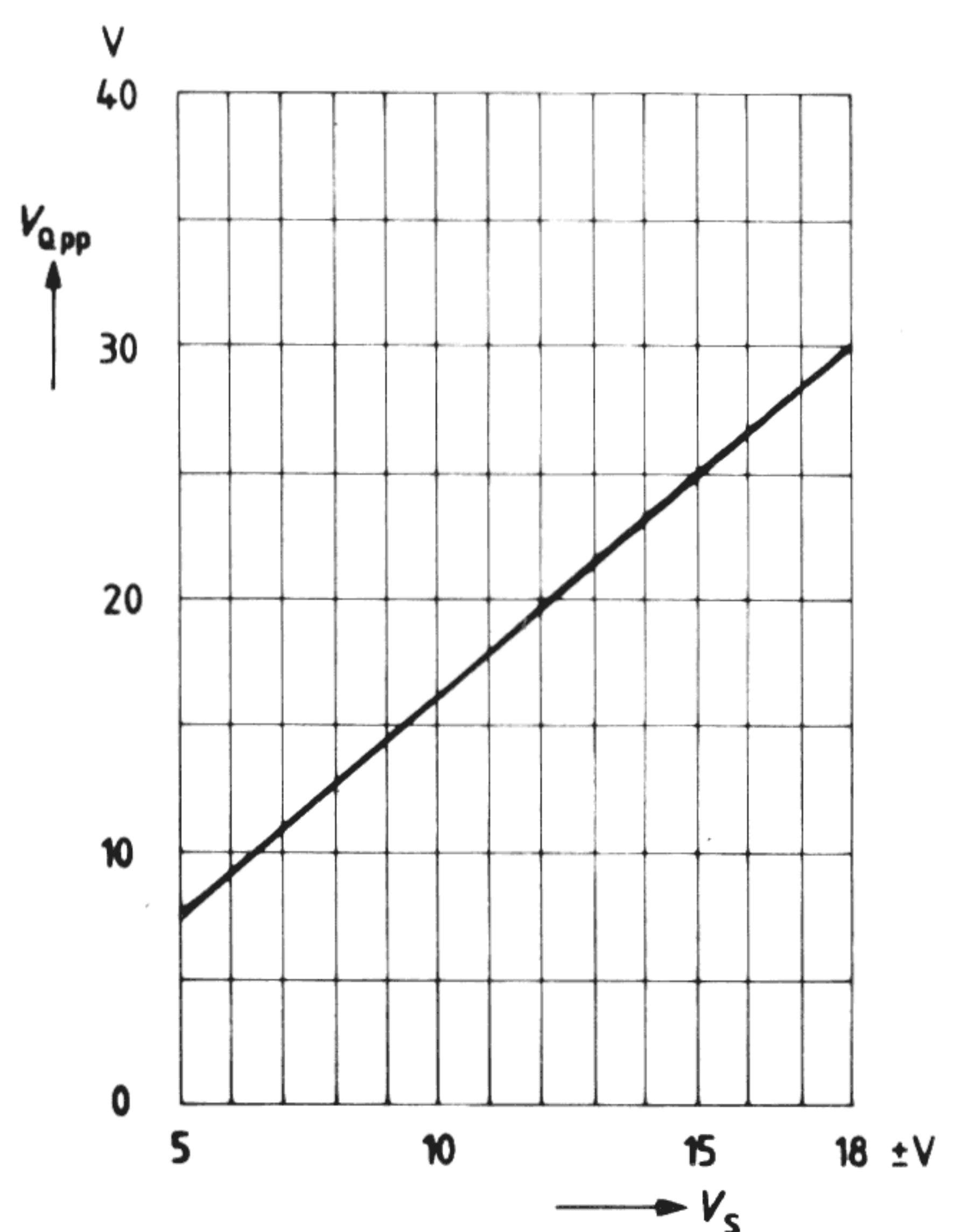
Input current $I_I = f(T_{\text{amb}})$



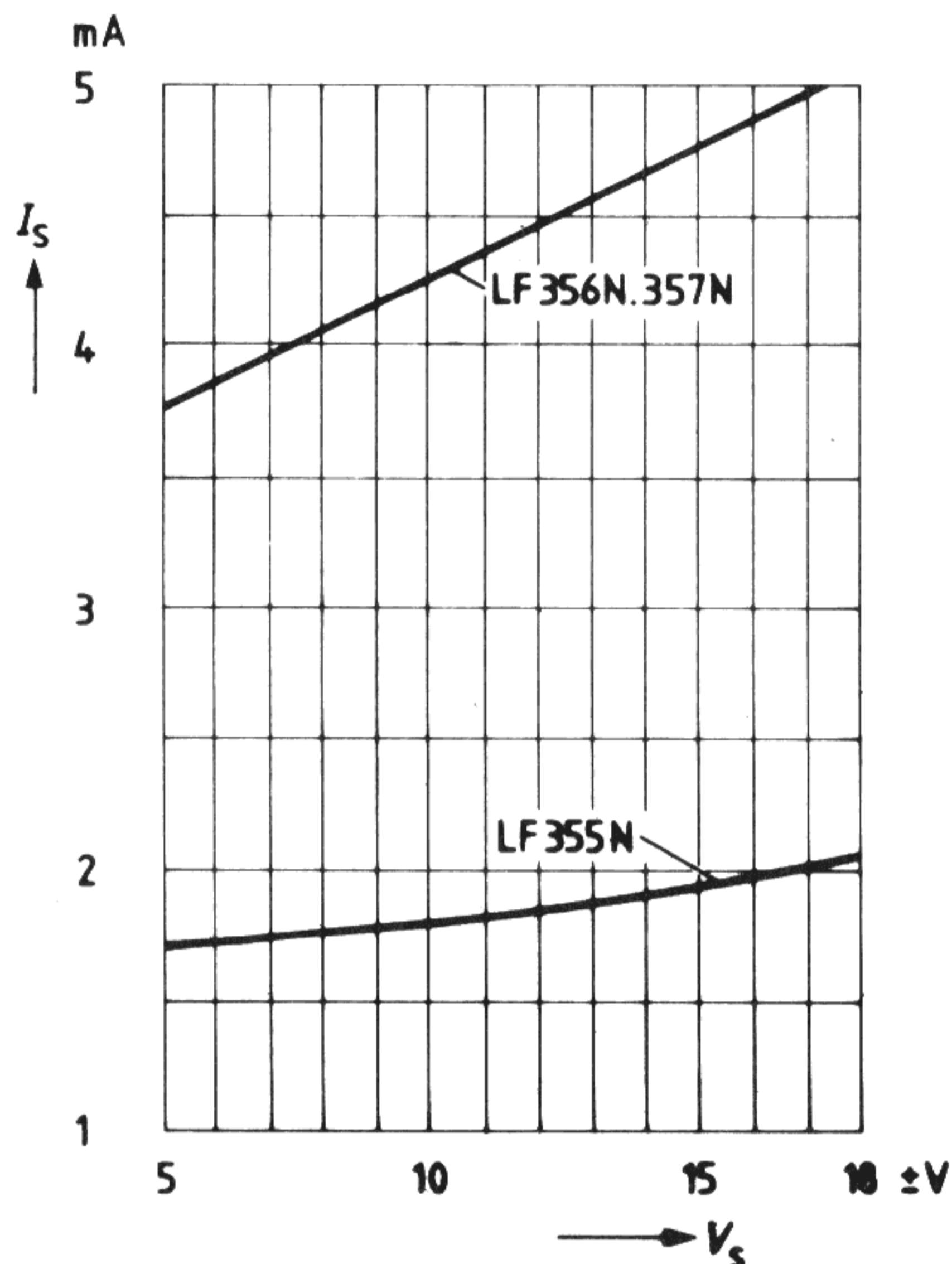
Input current $I_I = f(V_{IC})$
 $V_S = \pm 15V, T_{\text{amb}} = 25^\circ\text{C}$
 $R_L = 50\text{ k}\Omega$



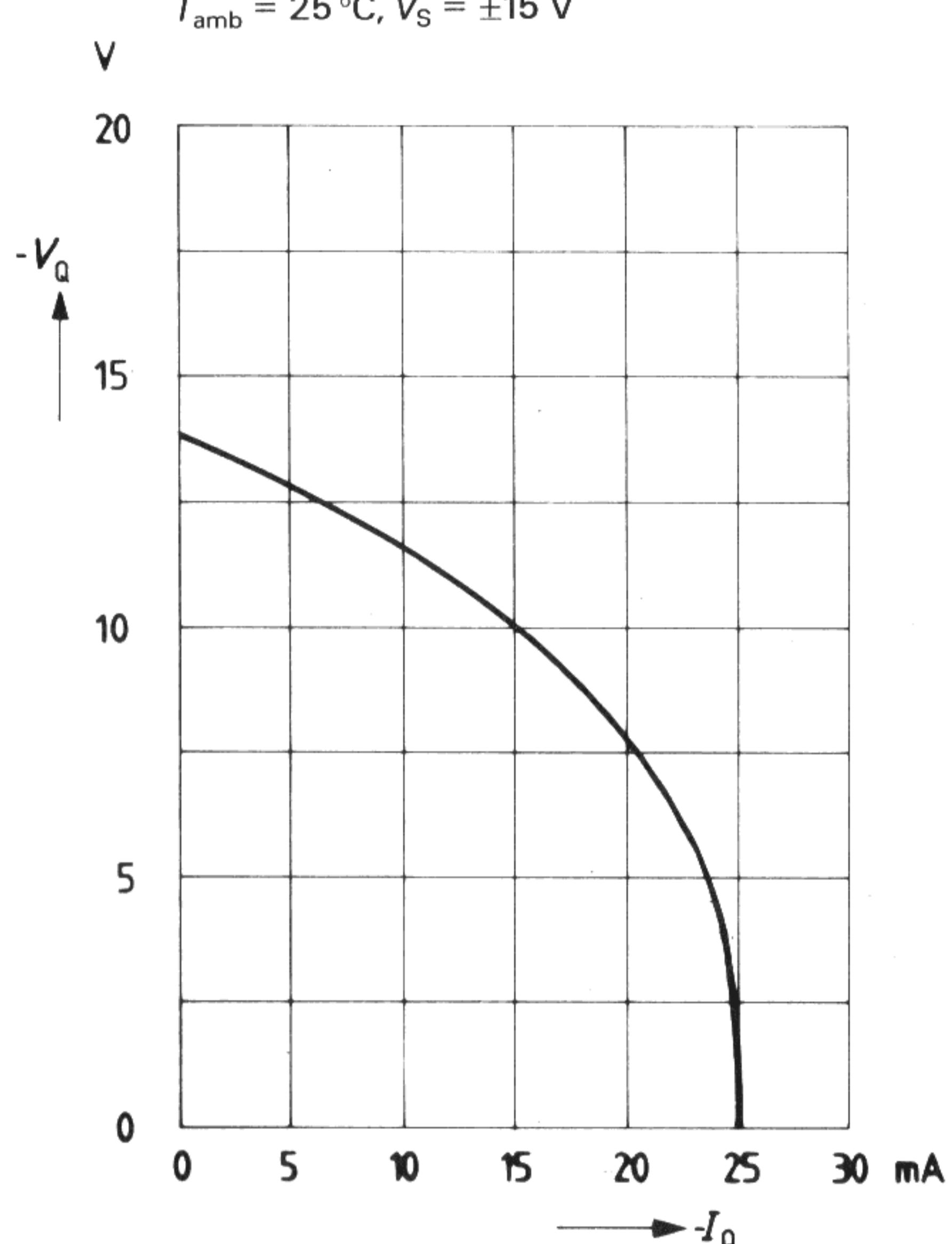
Output voltage $V_{QPP} = f(V_S)$
 $T_{\text{amb}} = 25^\circ\text{C}; R_L = 2\text{ k}\Omega$



Supply current $I_S = f(V_S)$

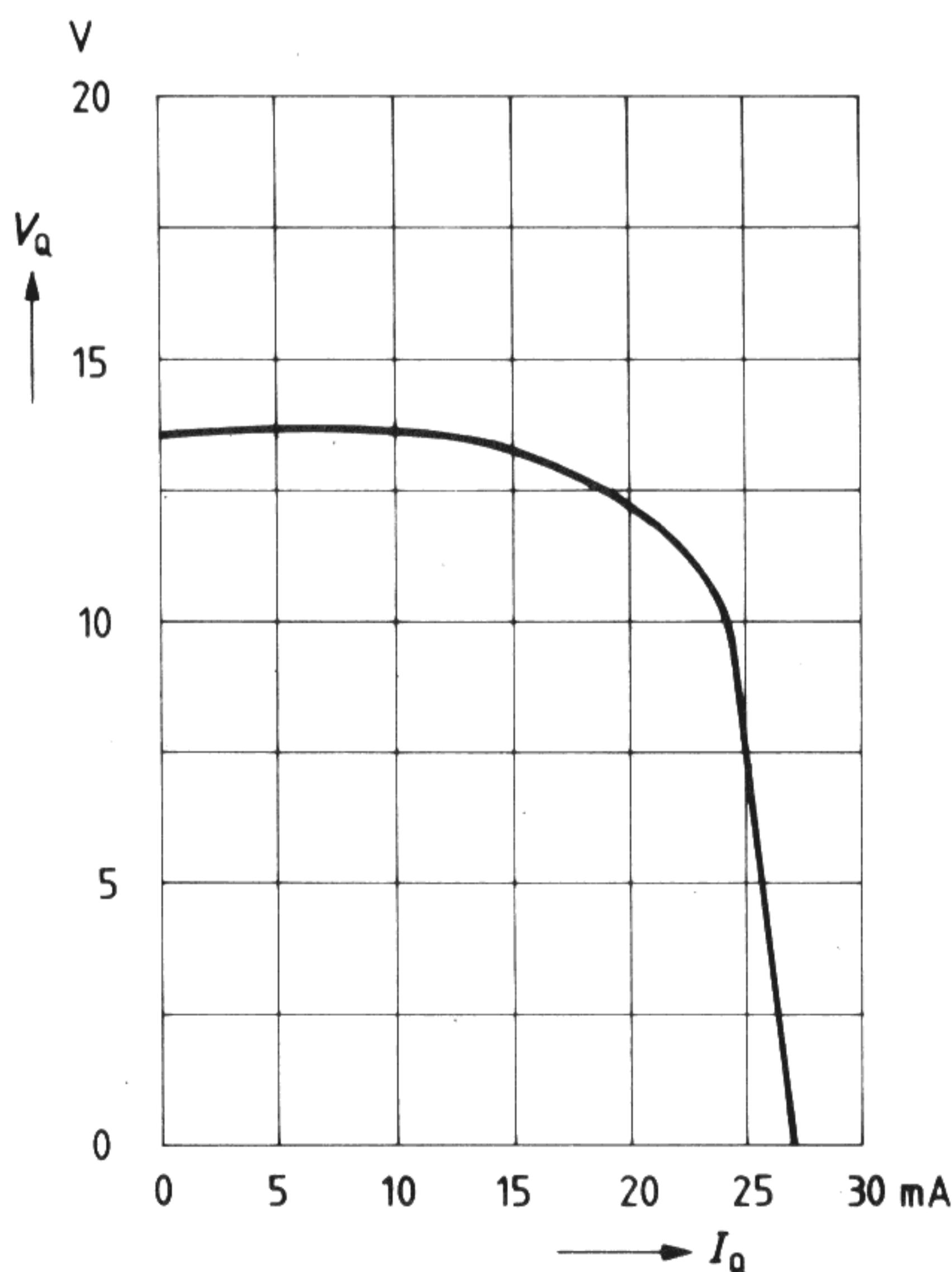


Negative short-circuit current



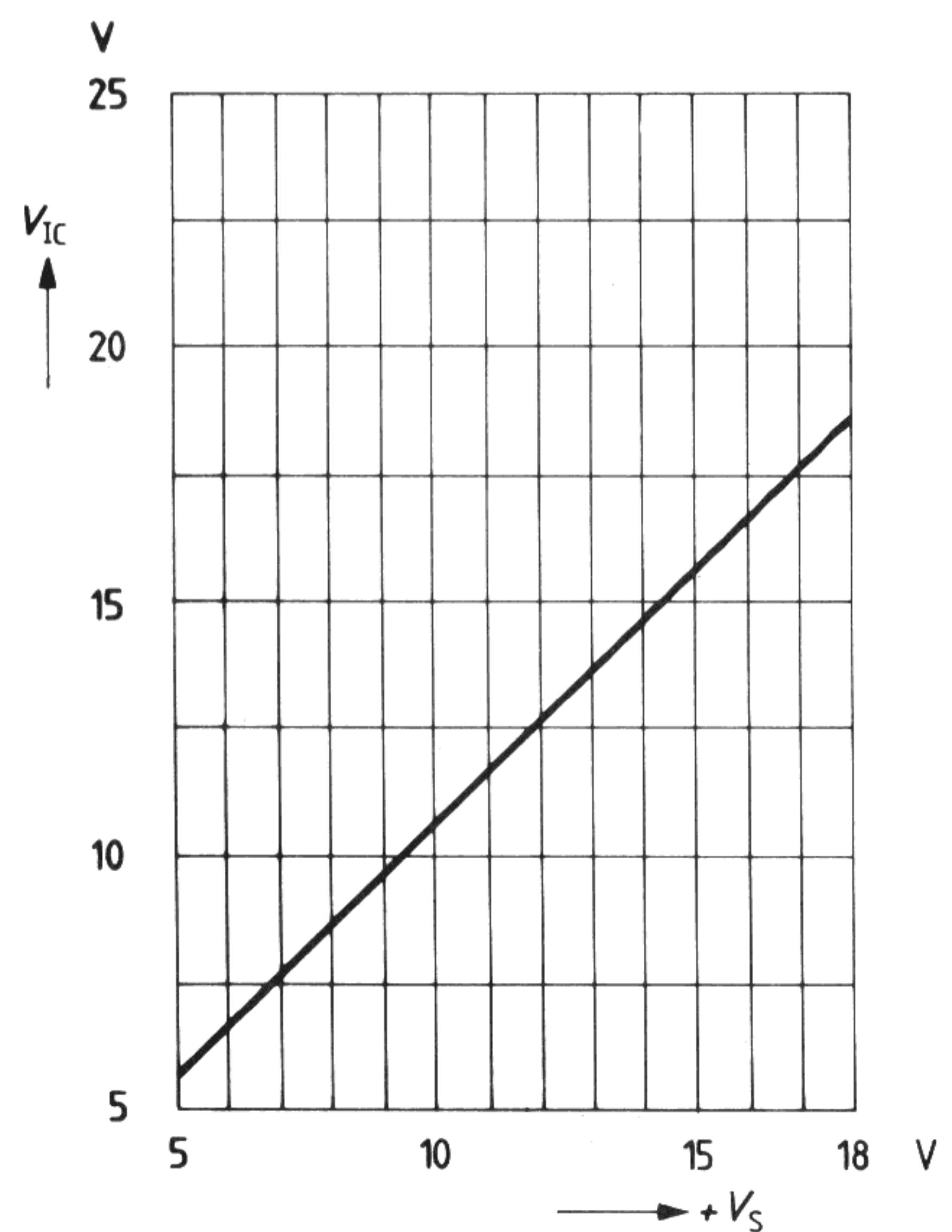
Positive short-circuit current

$V_Q = f(I_Q)$
 $T_{amb} = 25^\circ C, V_S = \pm 15 V$

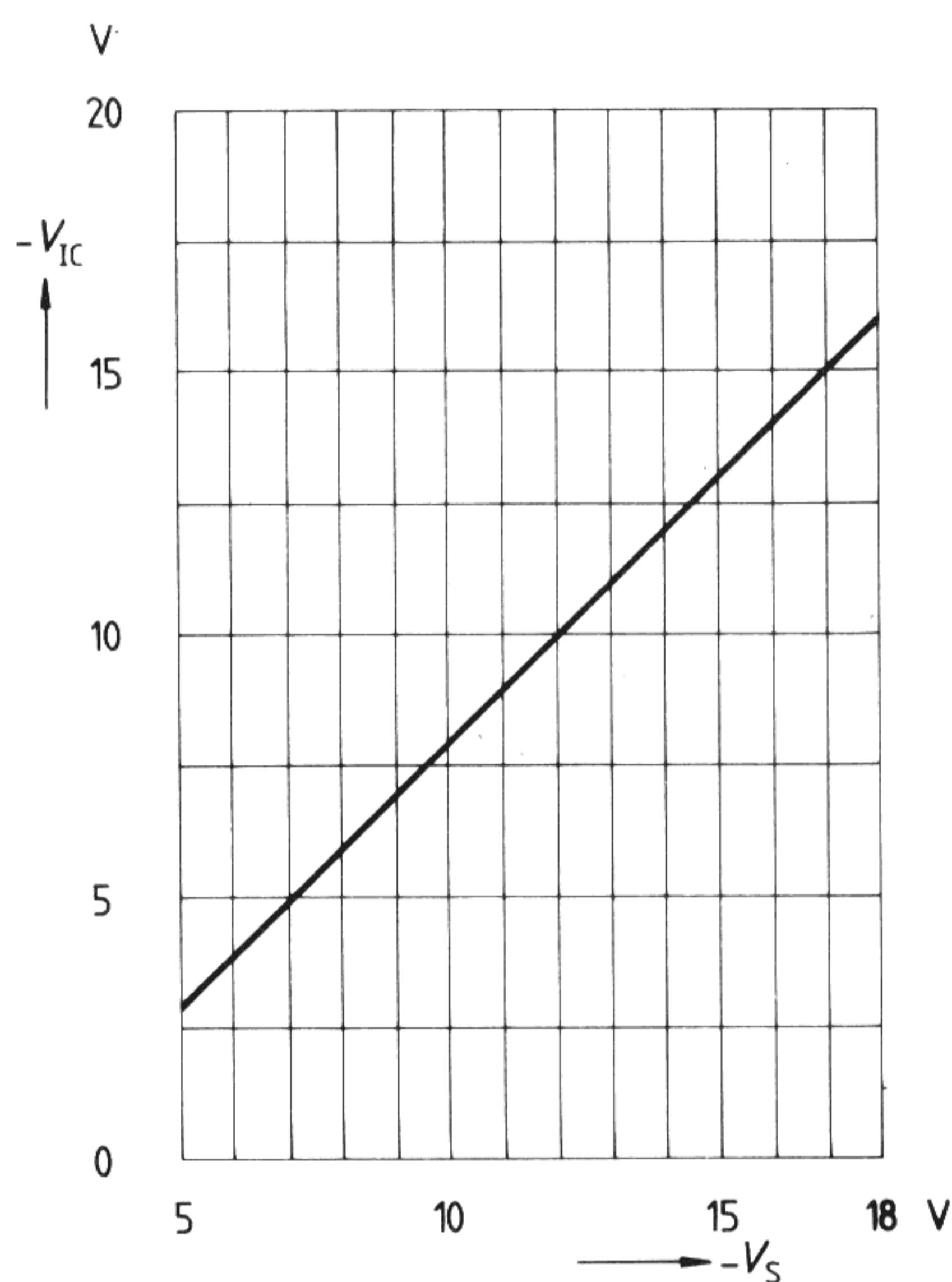


Positive input common mode voltage

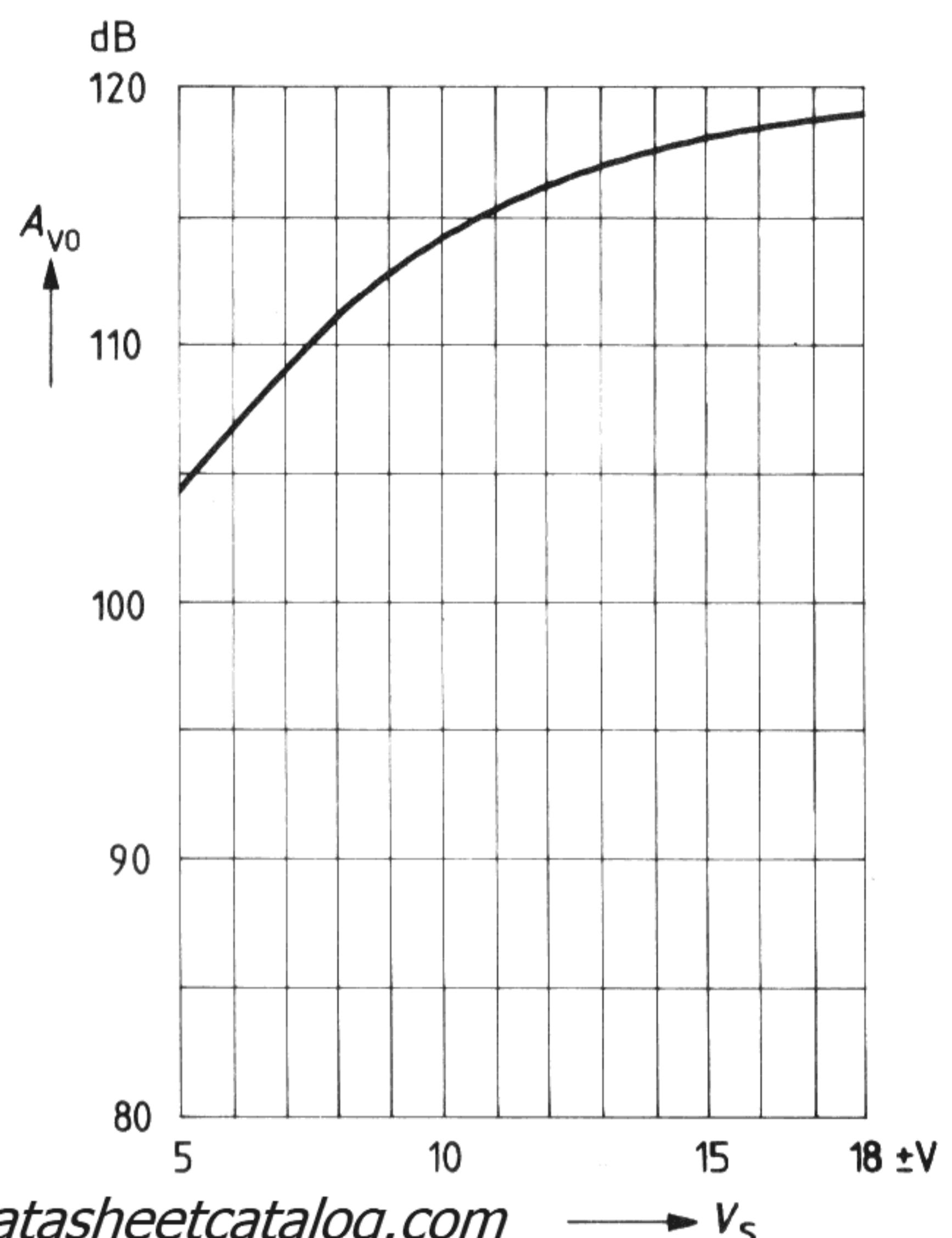
$V_{IC} = f(V_S)$
 $T_{amb} = 0$ to $70^\circ C$



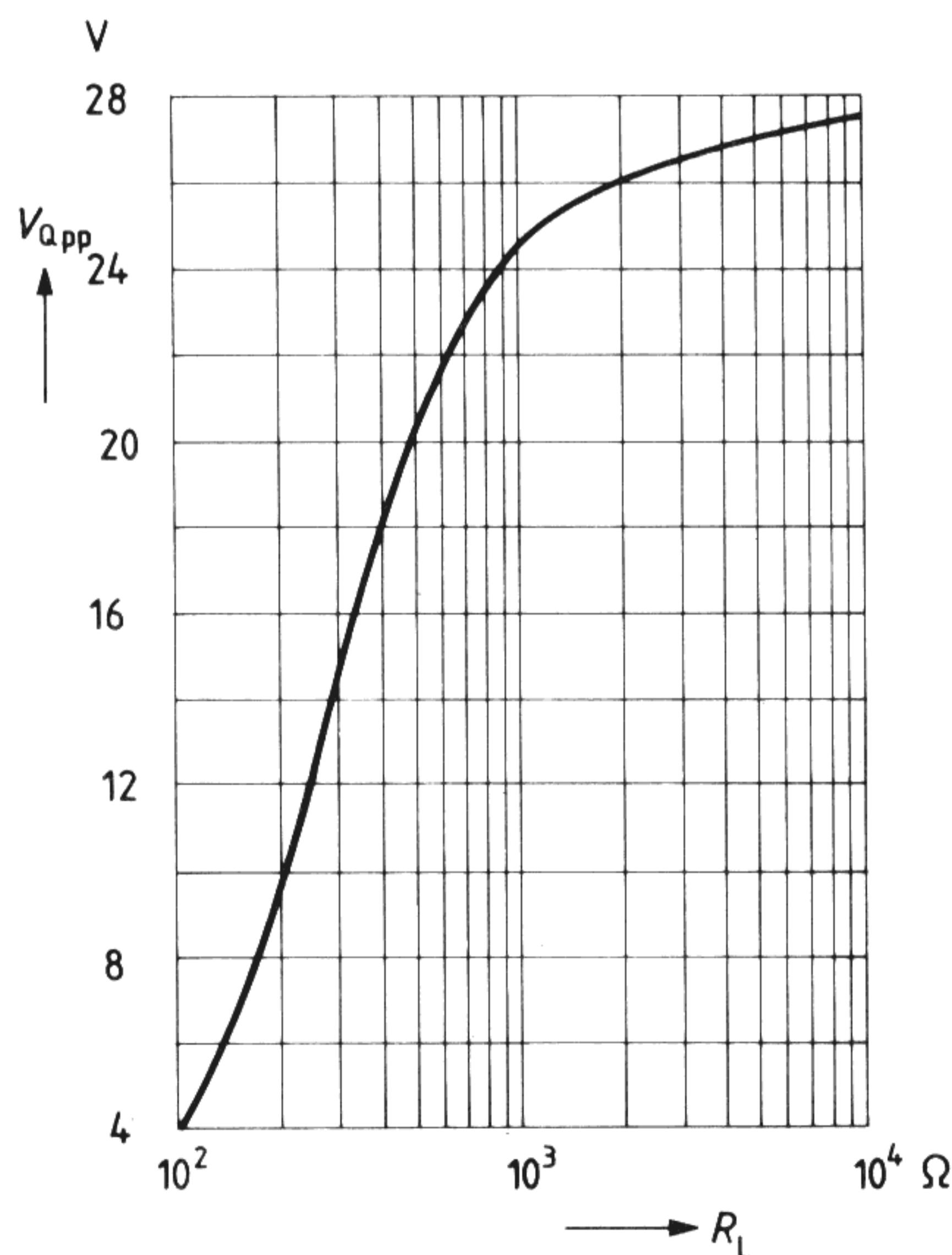
Negative input common mode voltage
 $-V_{IC} = f(-V_S); T_{amb} = 25^\circ C$



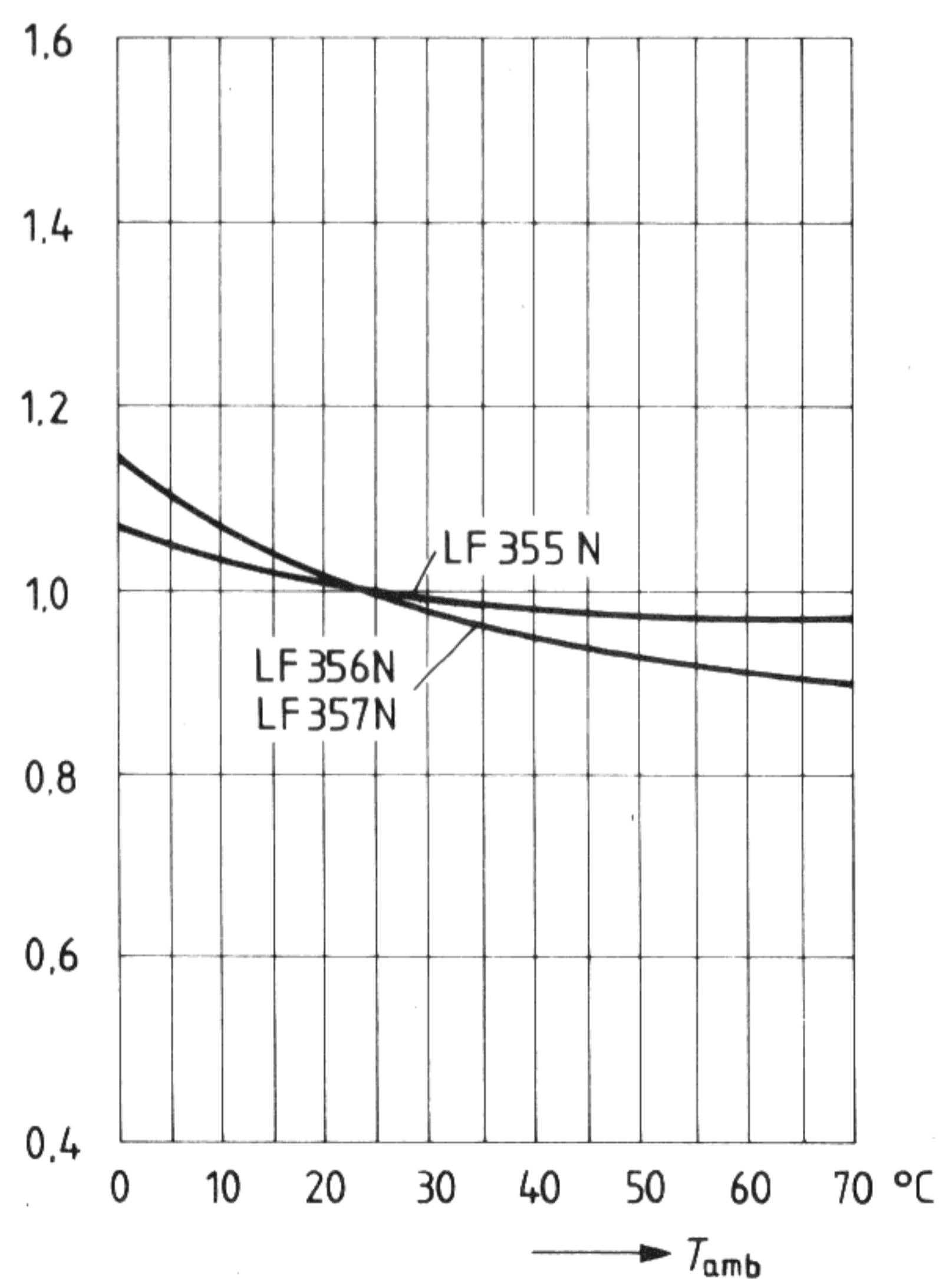
Open loop voltage amplification
 $A_{VO} = f(V_S)$
 $R_L = 2 k\Omega, R_G = 50 \Omega, T_{amb} = 25^\circ C$



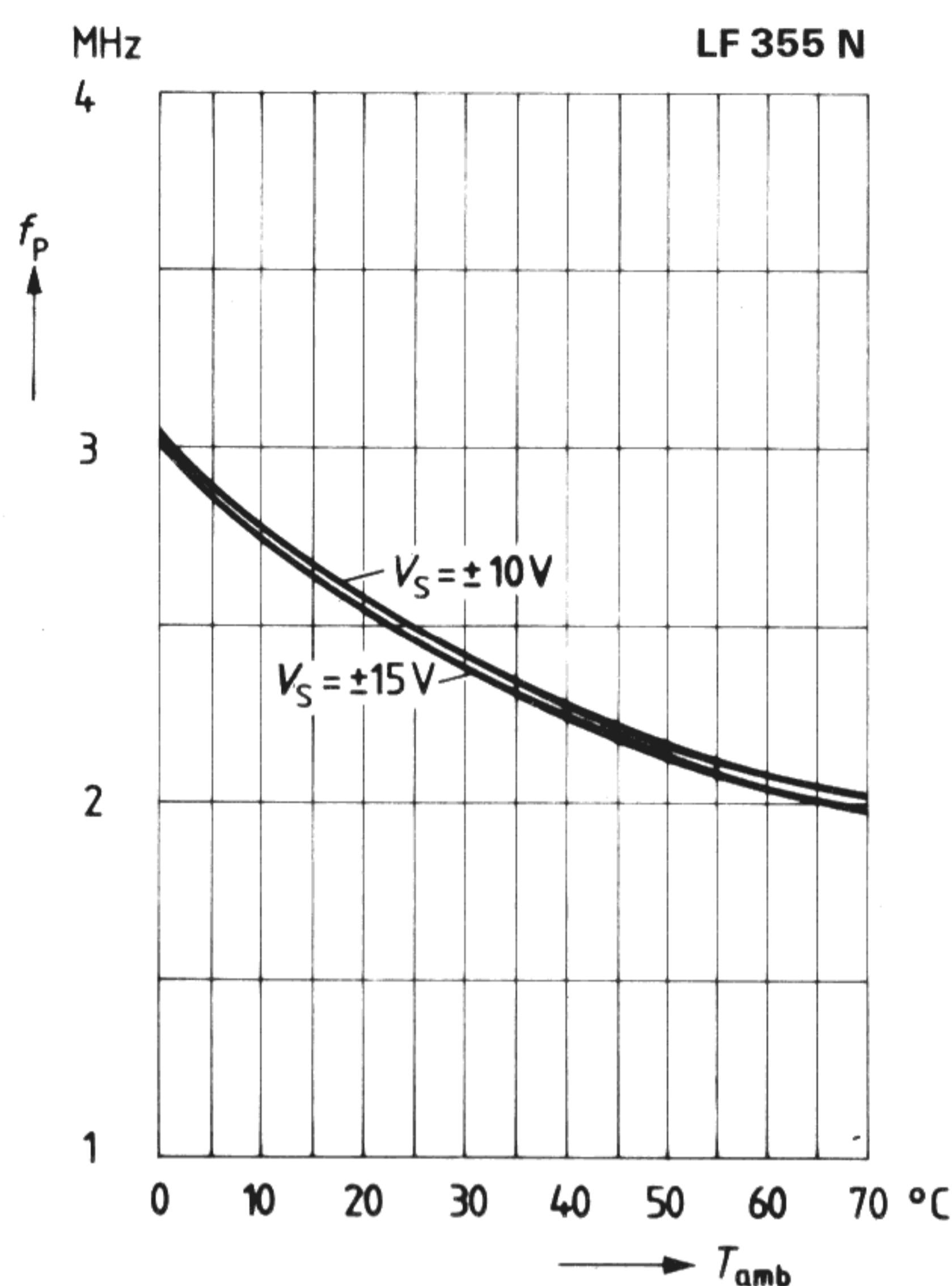
Output voltage V_{Opp} = $f(R_L)$
 $V_S = \pm 15 V; T_{amb} = 25^\circ C$



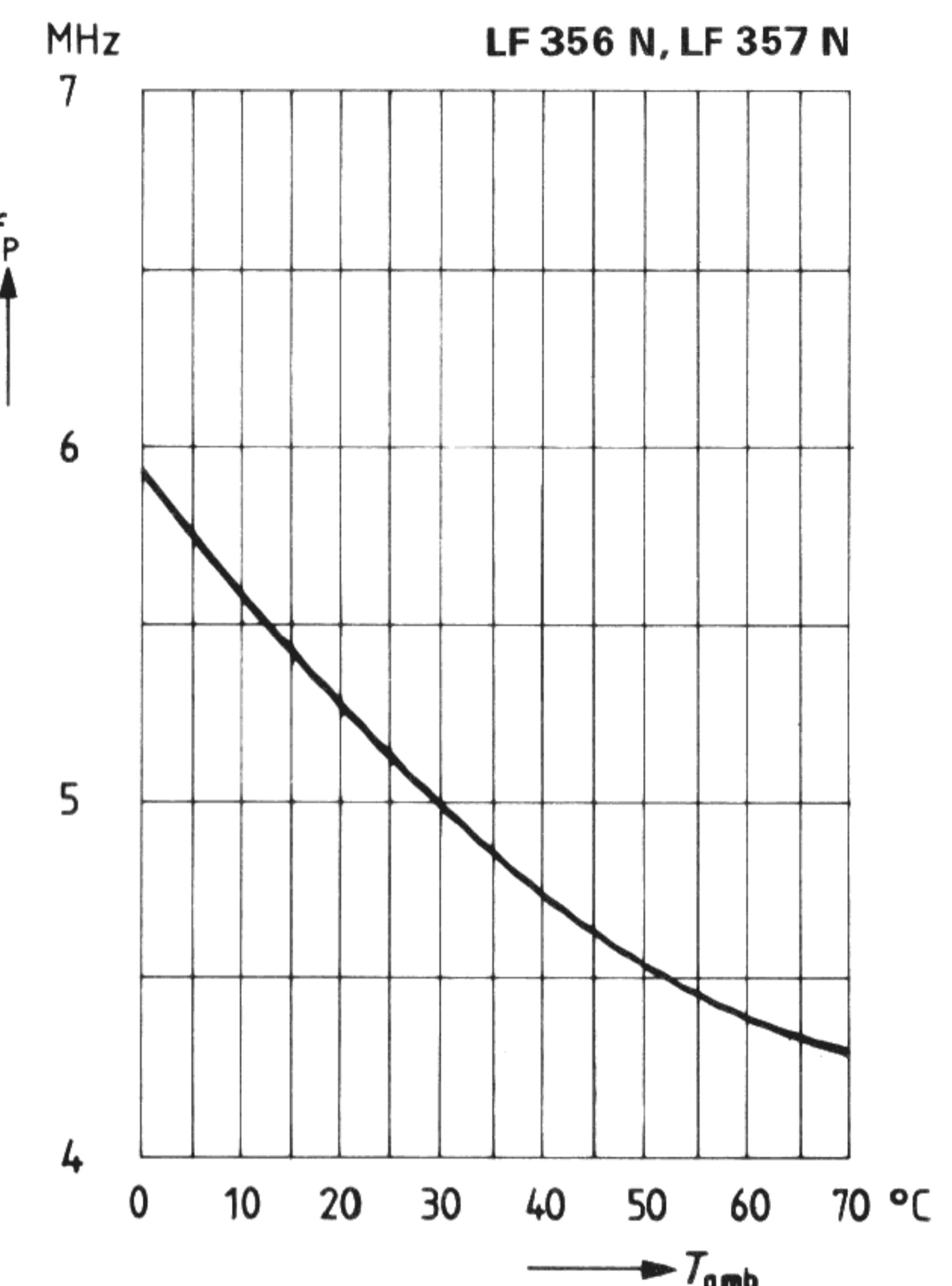
Standardized rise time
 $V_S = \pm 15 V$



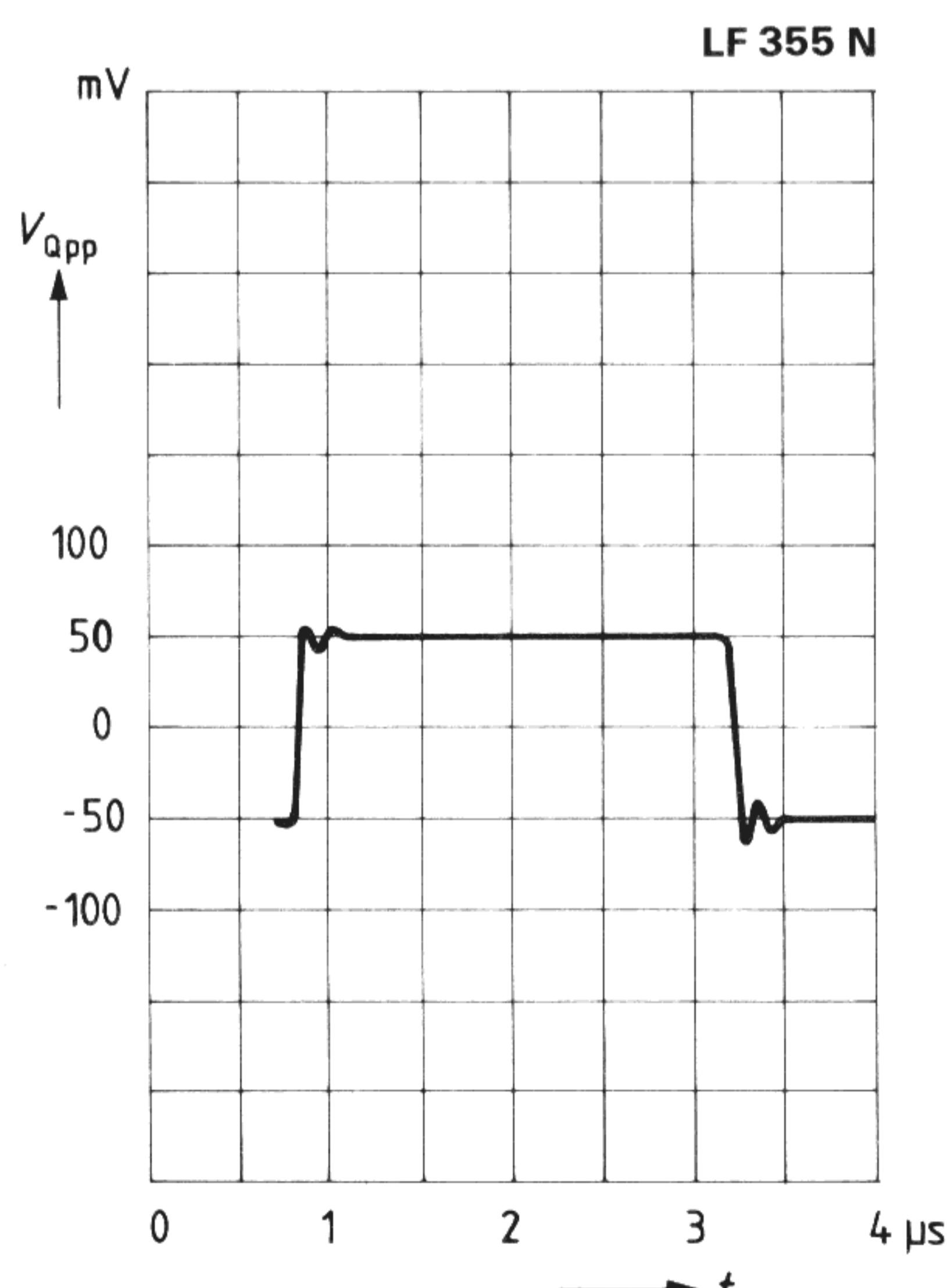
Performance bandwidth $f_p = f(T_{amb})$



Performance bandwidth $f_p = f(T_{amb})$, $A_V = 1$

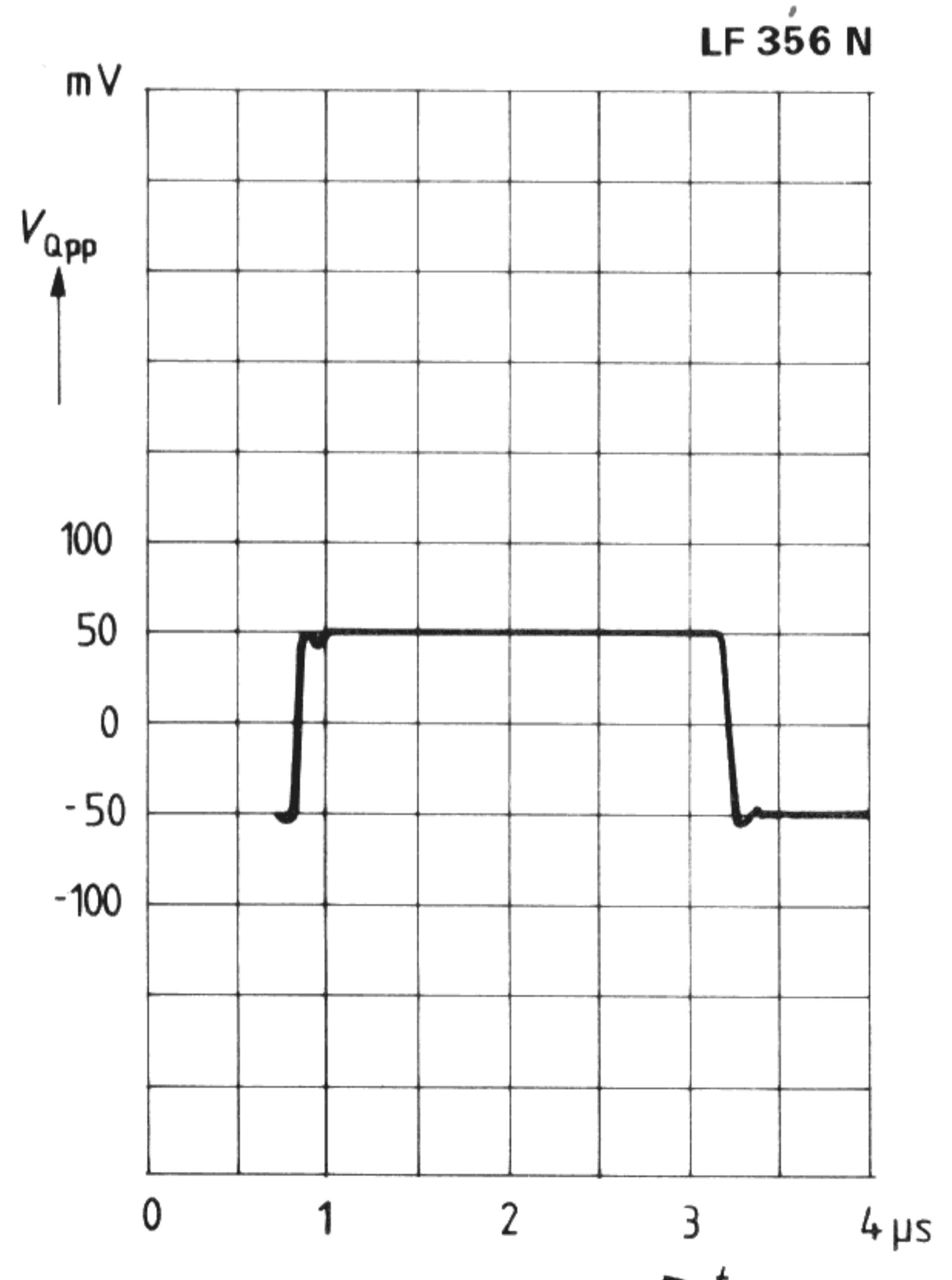


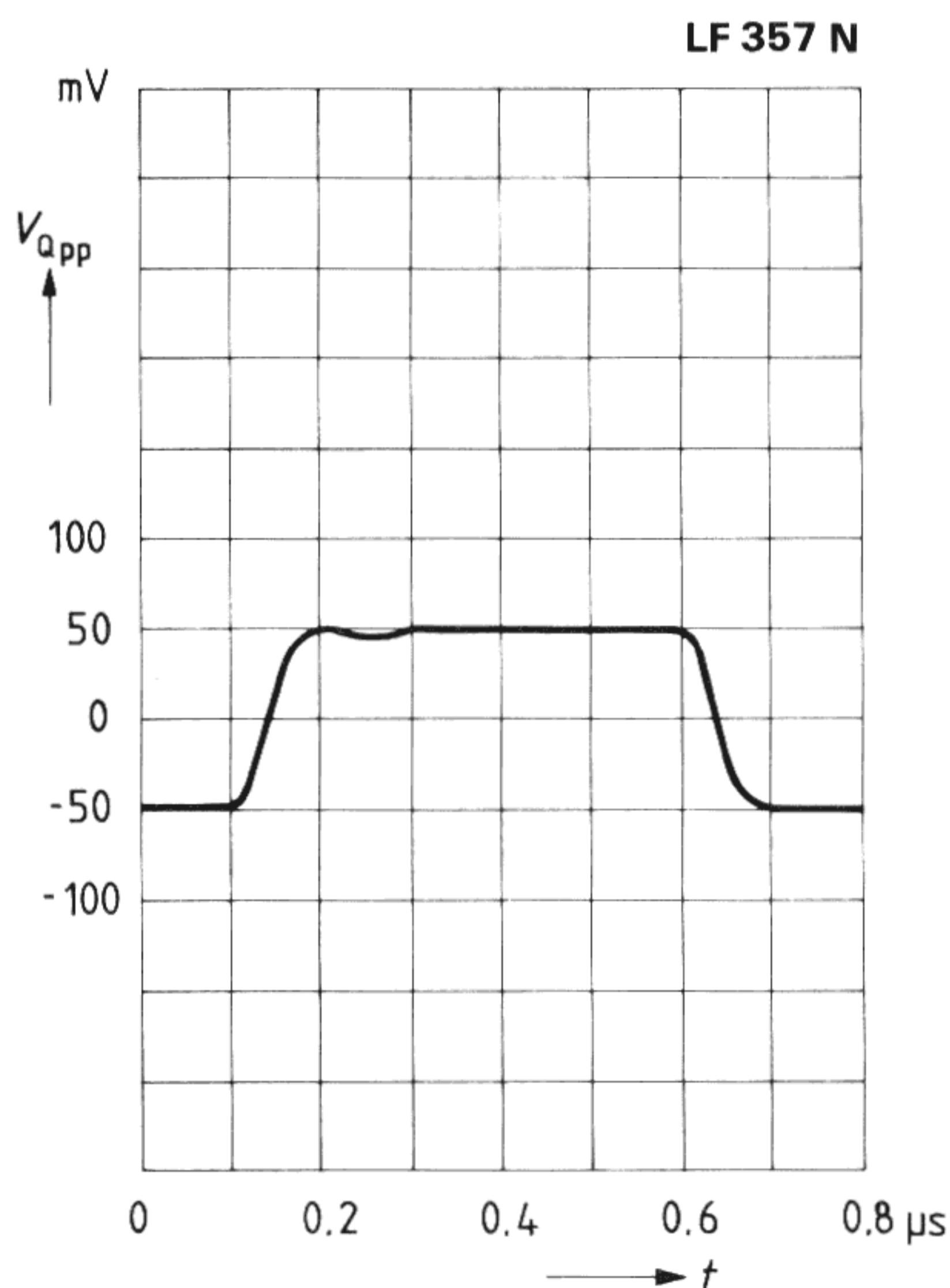
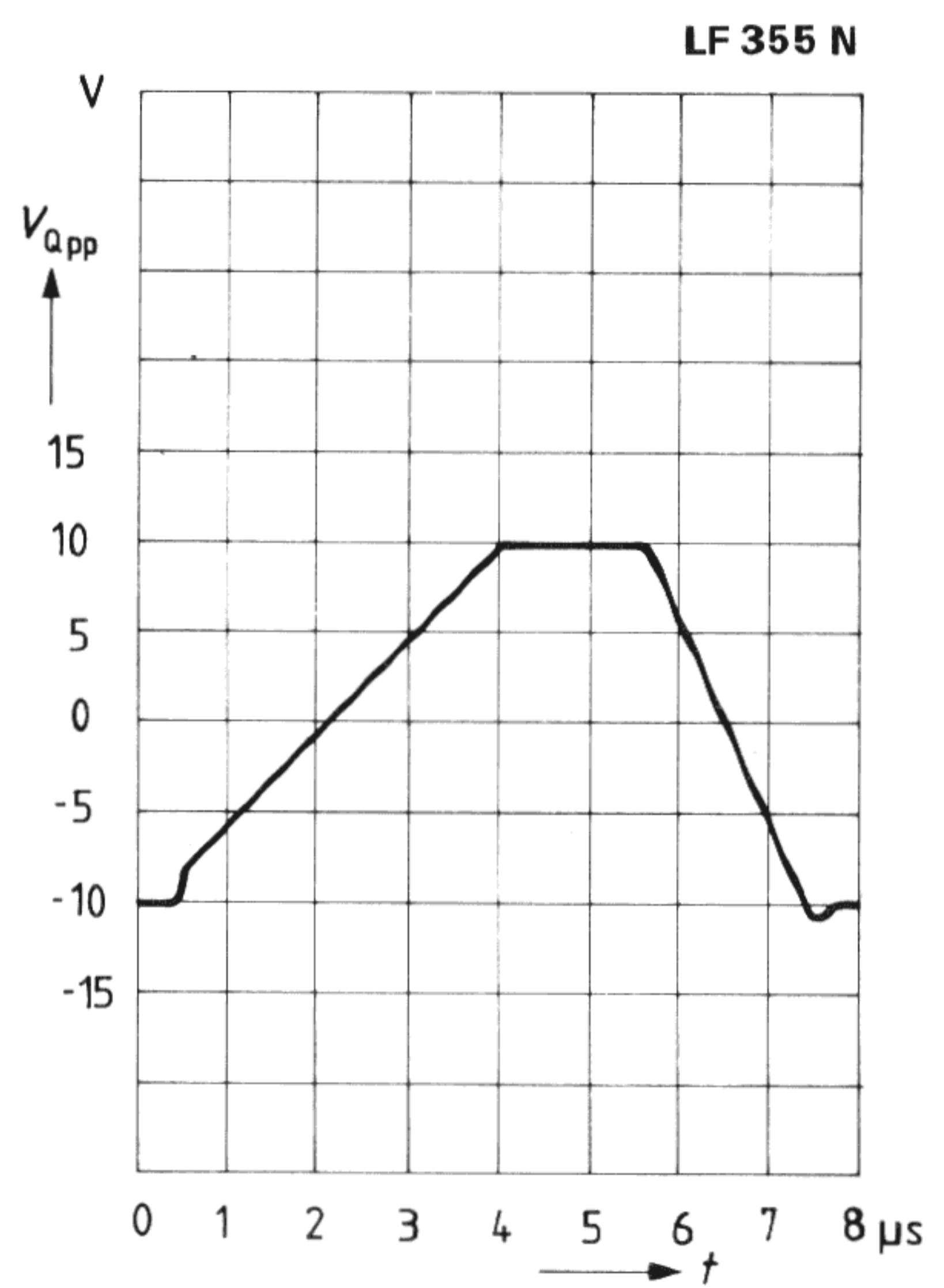
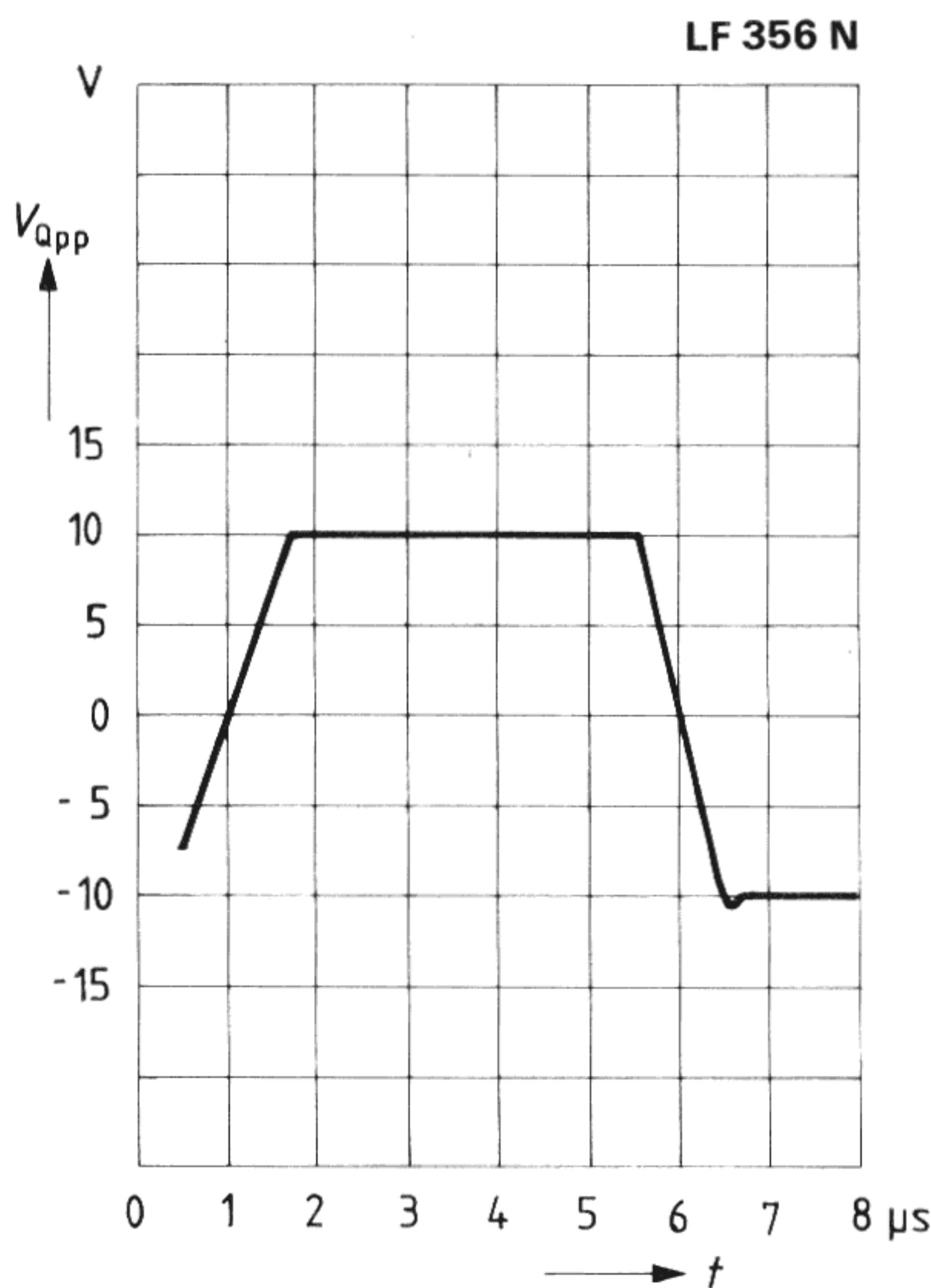
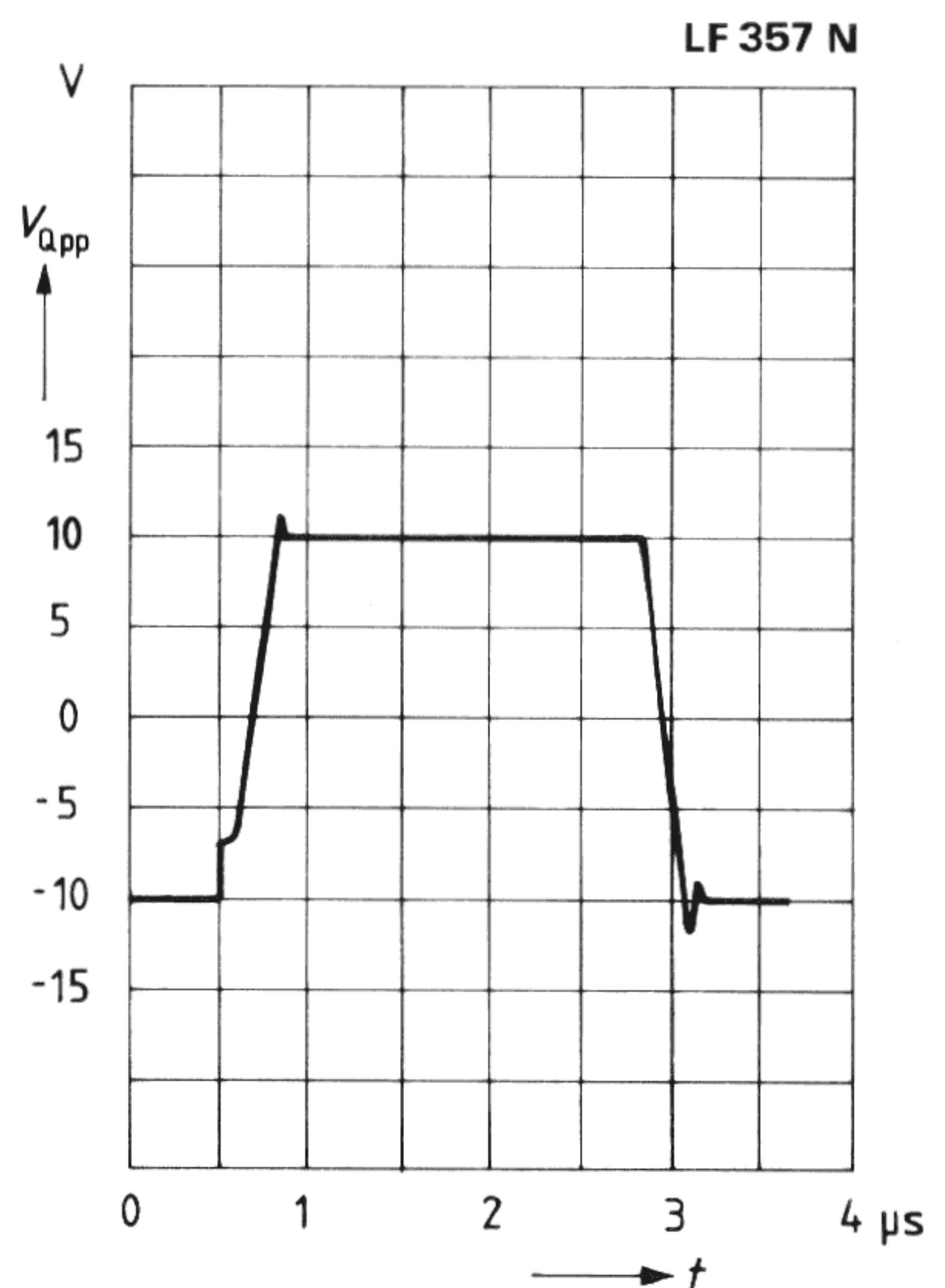
Small signal response $A_V = 1$



The curves for LF 357 N are multiplied by the factor 4.

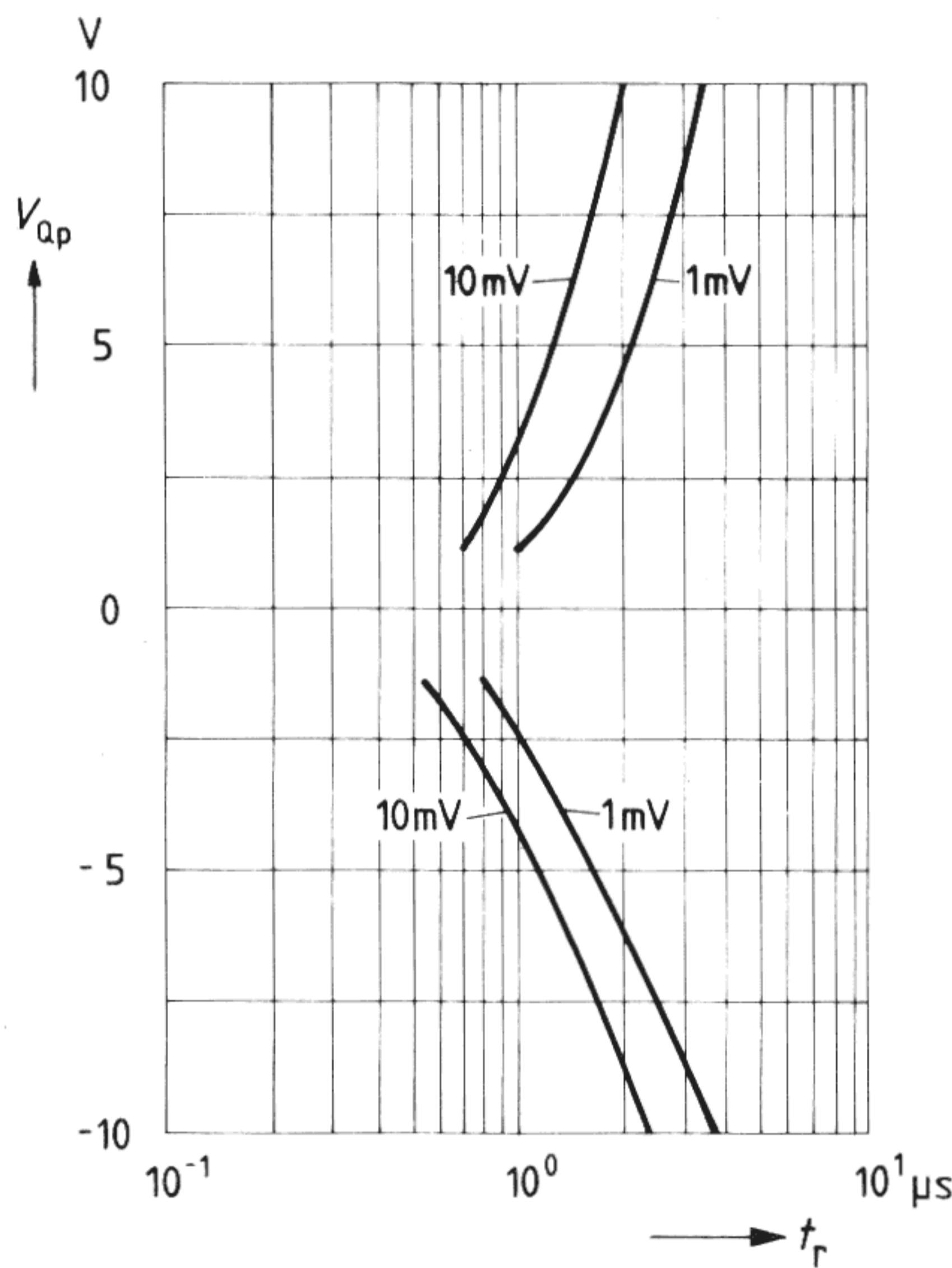
Small signal response $A_V = 1$



Small signal response $A_V = 5$ Large-signal response $A_V = 1$ Large-signal response $A_V = 1$ Large-signal response $A_V = 5$ 

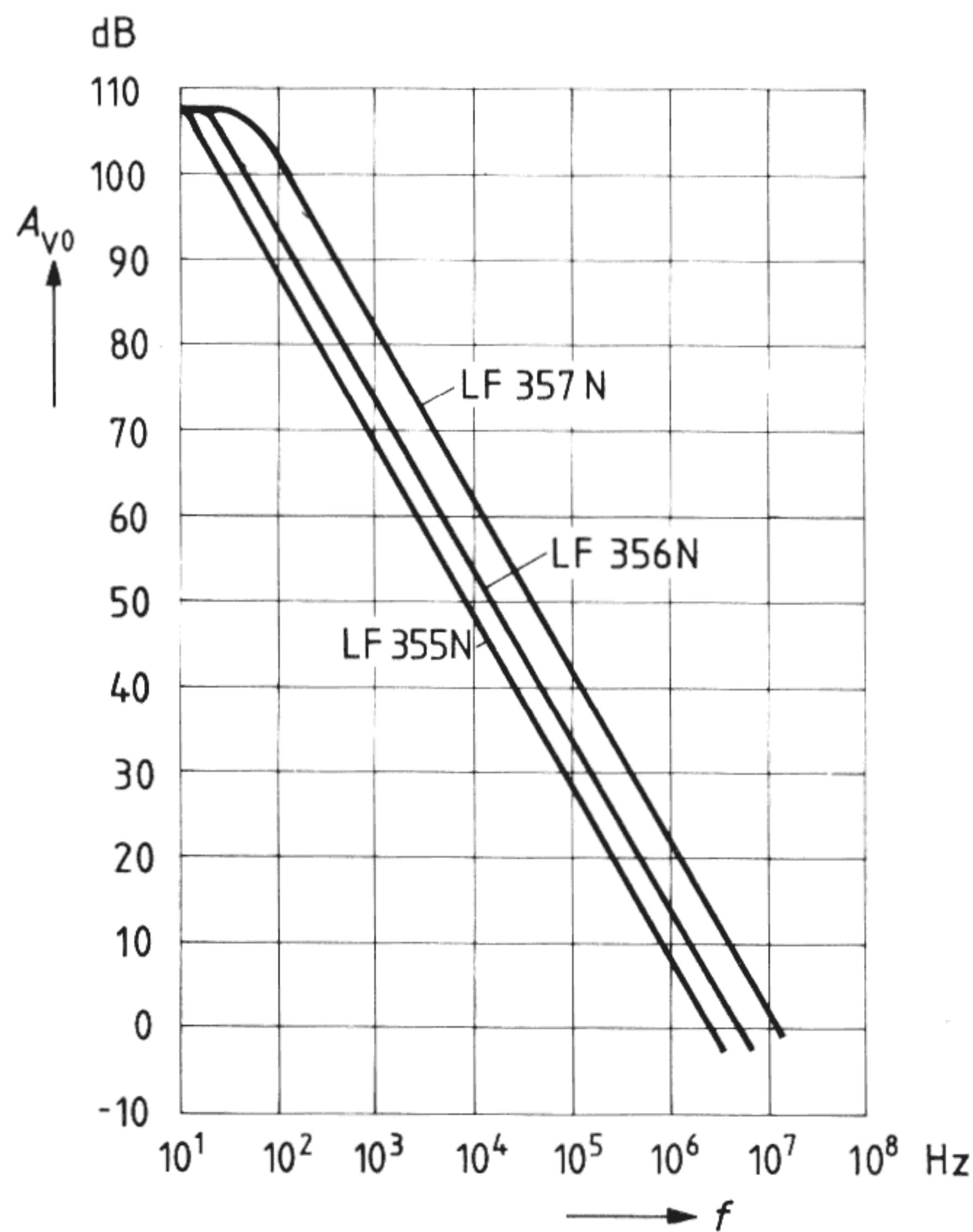
Transient time of inverter

LF 355 N; $V_S = \pm 15$ V,
 $T_{amb} = 25$ °C



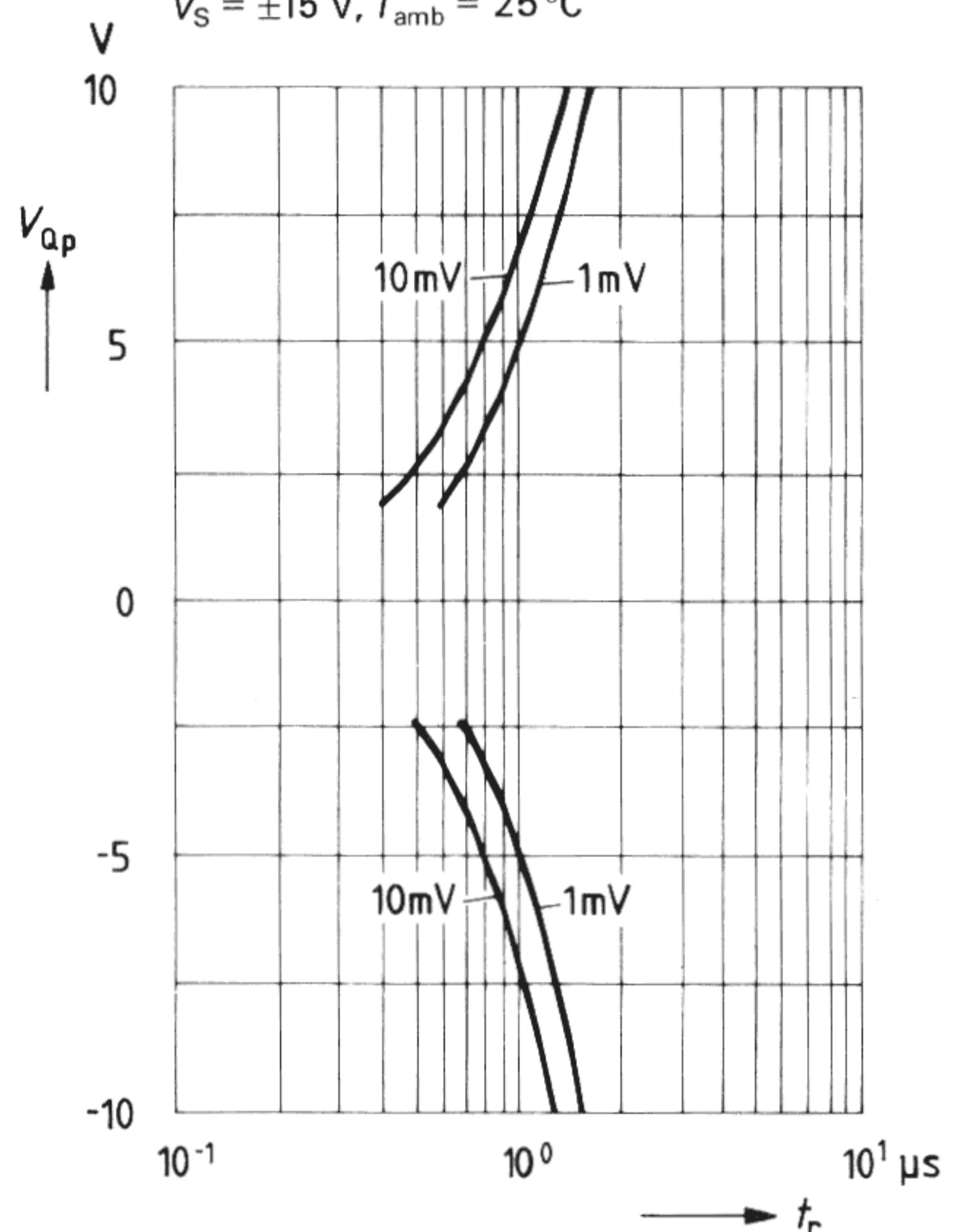
Open-loop voltage amplification

$A_{VO} = f(f)$
 $V_S = \pm 15$ V



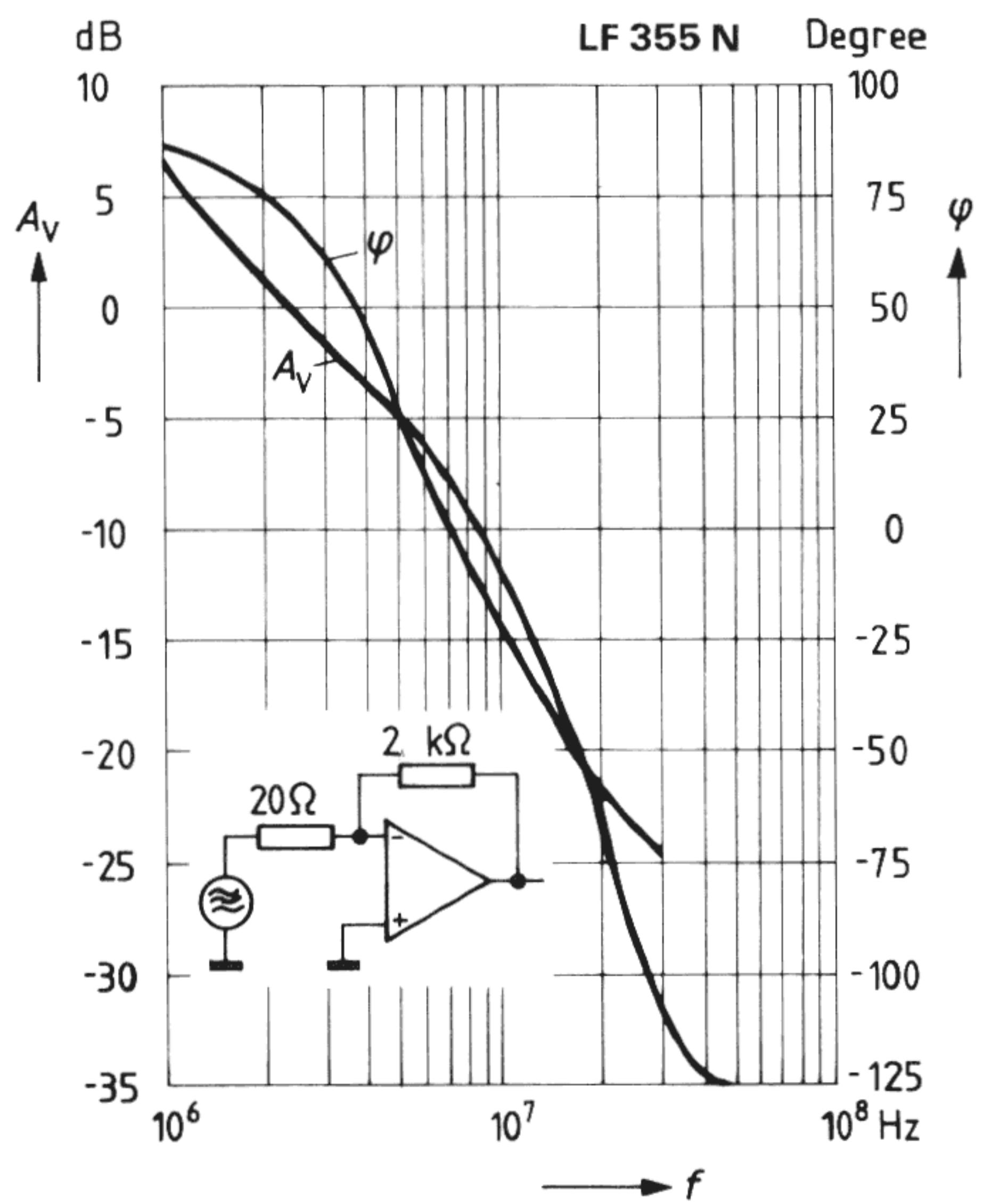
Transient time of inverter

LF 356 N; $A_V = -1$
 LF 357 N; $A_V = -5$
 $V_S = \pm 15$ V, $T_{amb} = 25$ °C



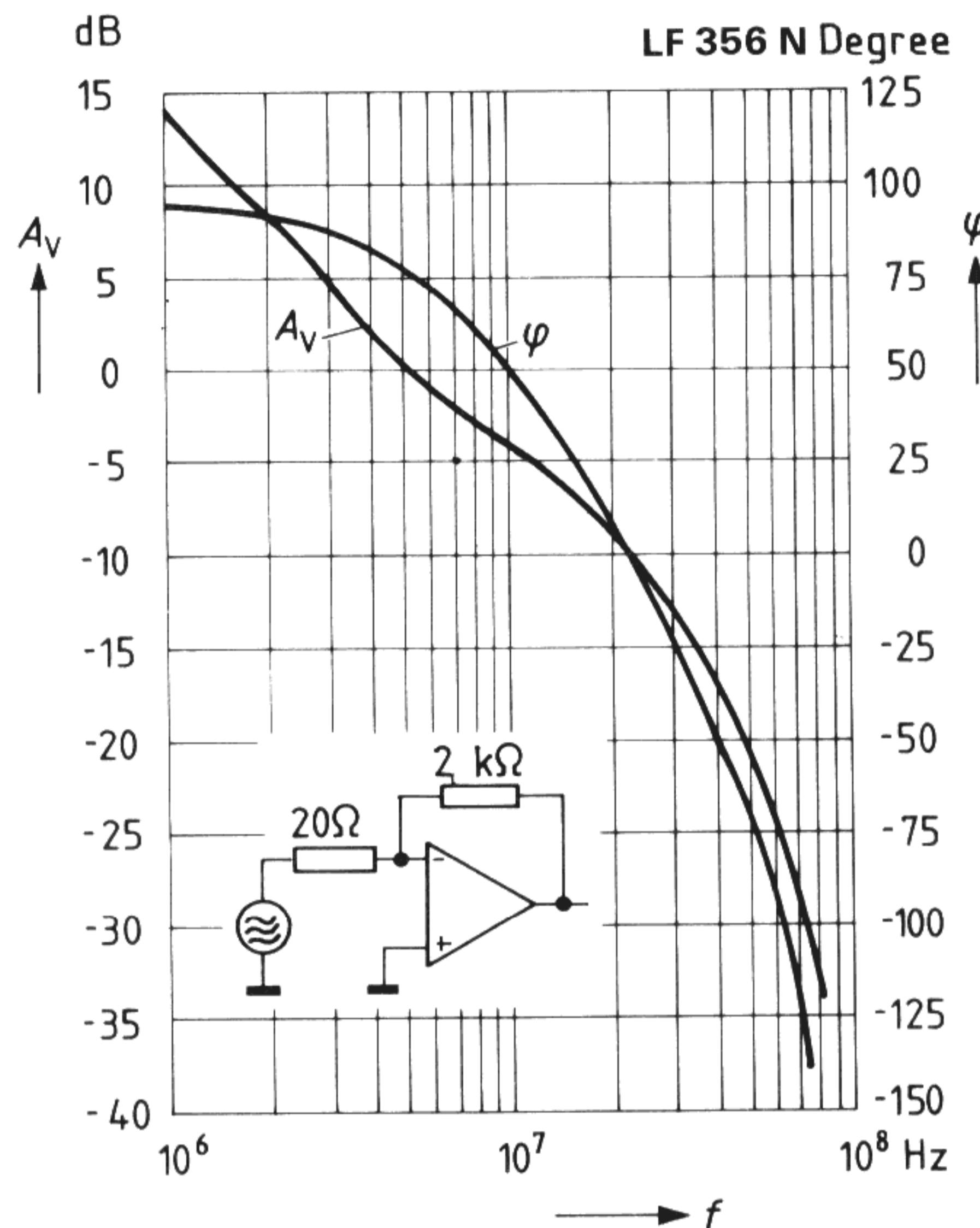
Bode diagram

$A_V = f(f)$ or $\varphi = f(f)$
 $V_S = \pm 15$ V



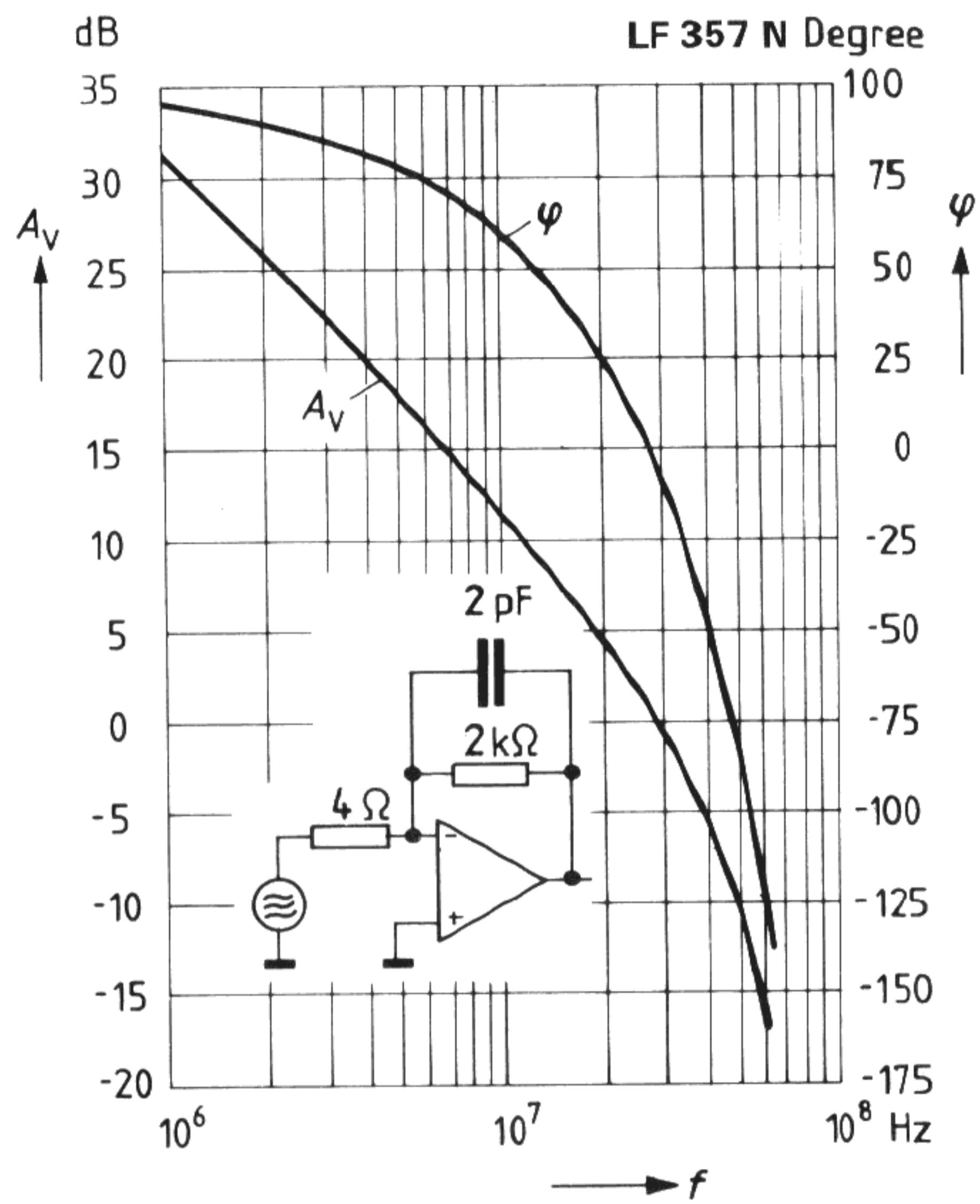
Bode diagram

$A_V = f(f)$ or $\varphi = f(f)$
 $V_S = \pm 15$ V



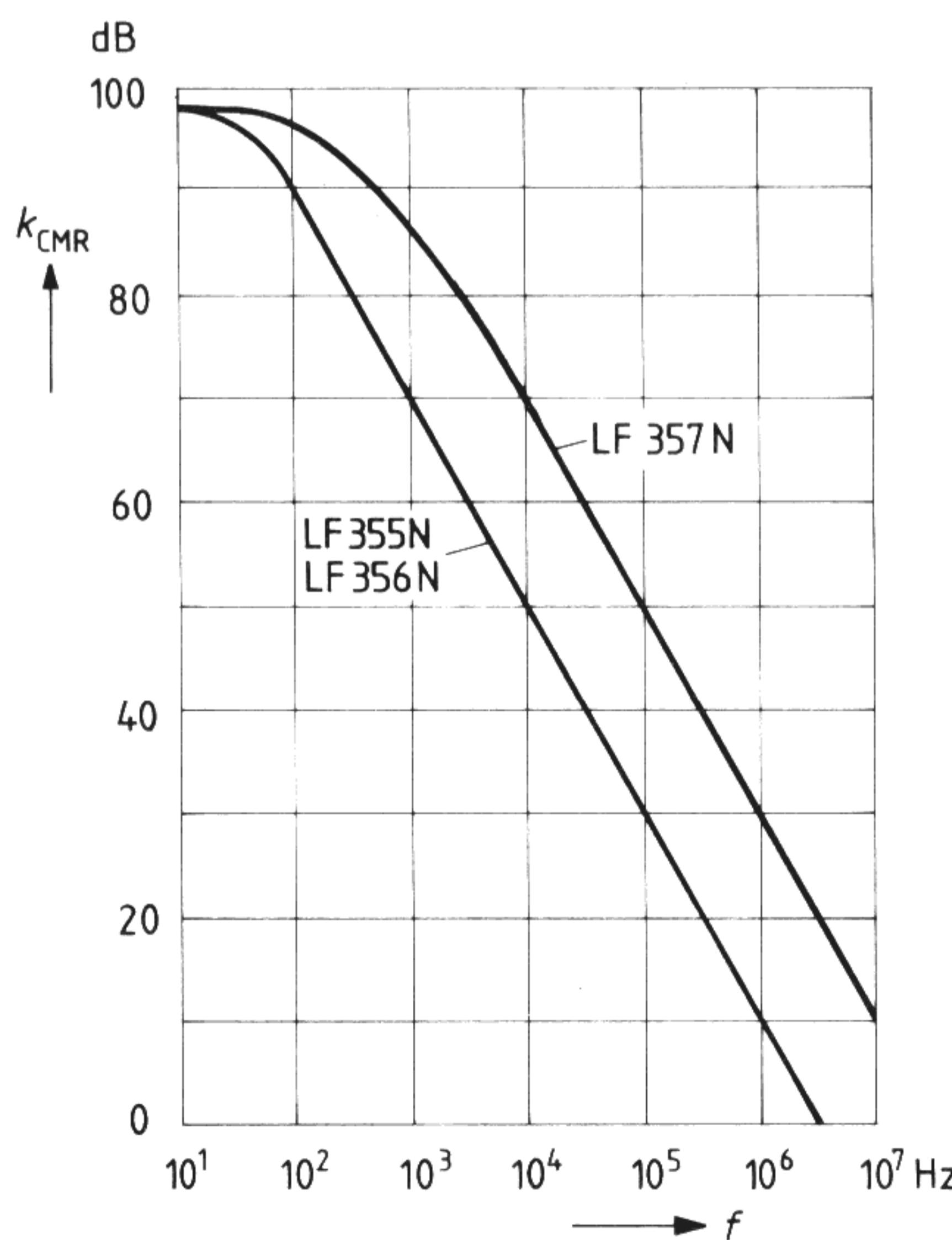
Bode diagram

$A_V = f(f)$ or $\varphi = f(f)$
 $V_S = \pm 15$ V



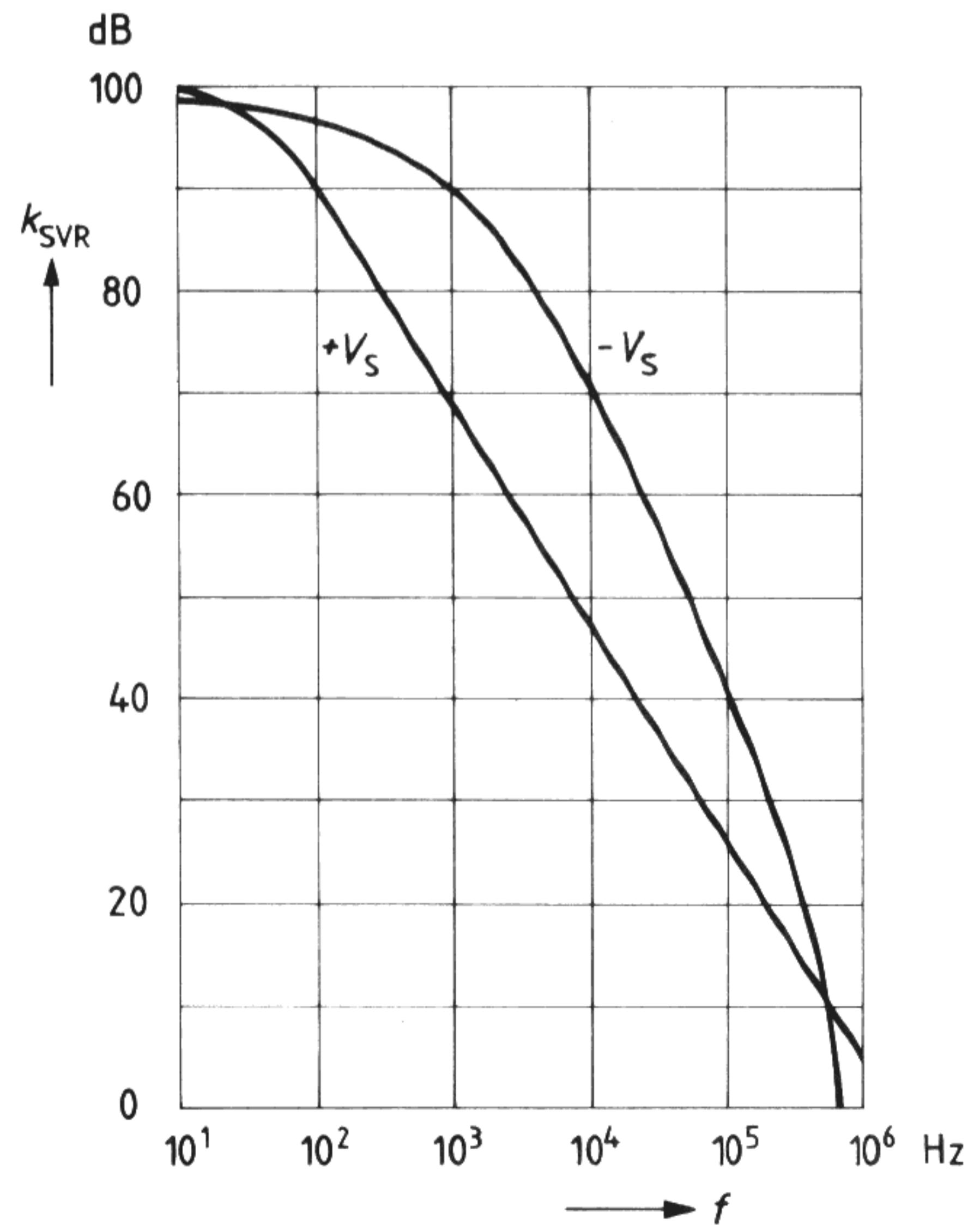
Common mode rejection

$k_{CMR} = f(f)$, $R_L = 2\text{ k}\Omega$
 $V_S = \pm 15$ V, $T_{amb} = 25^\circ C$



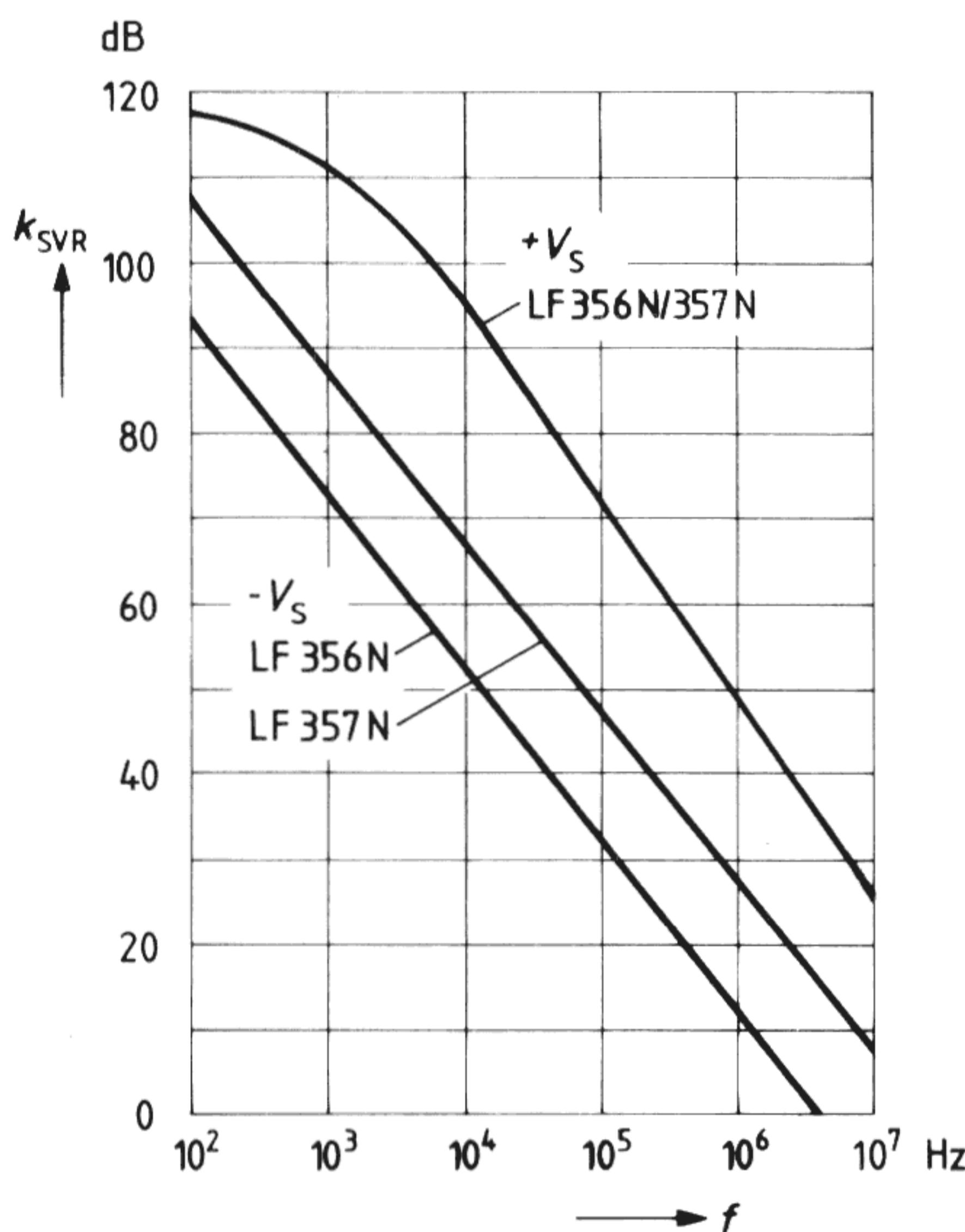
Supply voltage rejection

$k_{SVR} = f(f)$
 $V_S = \pm 15$ V; $T_{amb} = 25^\circ C$



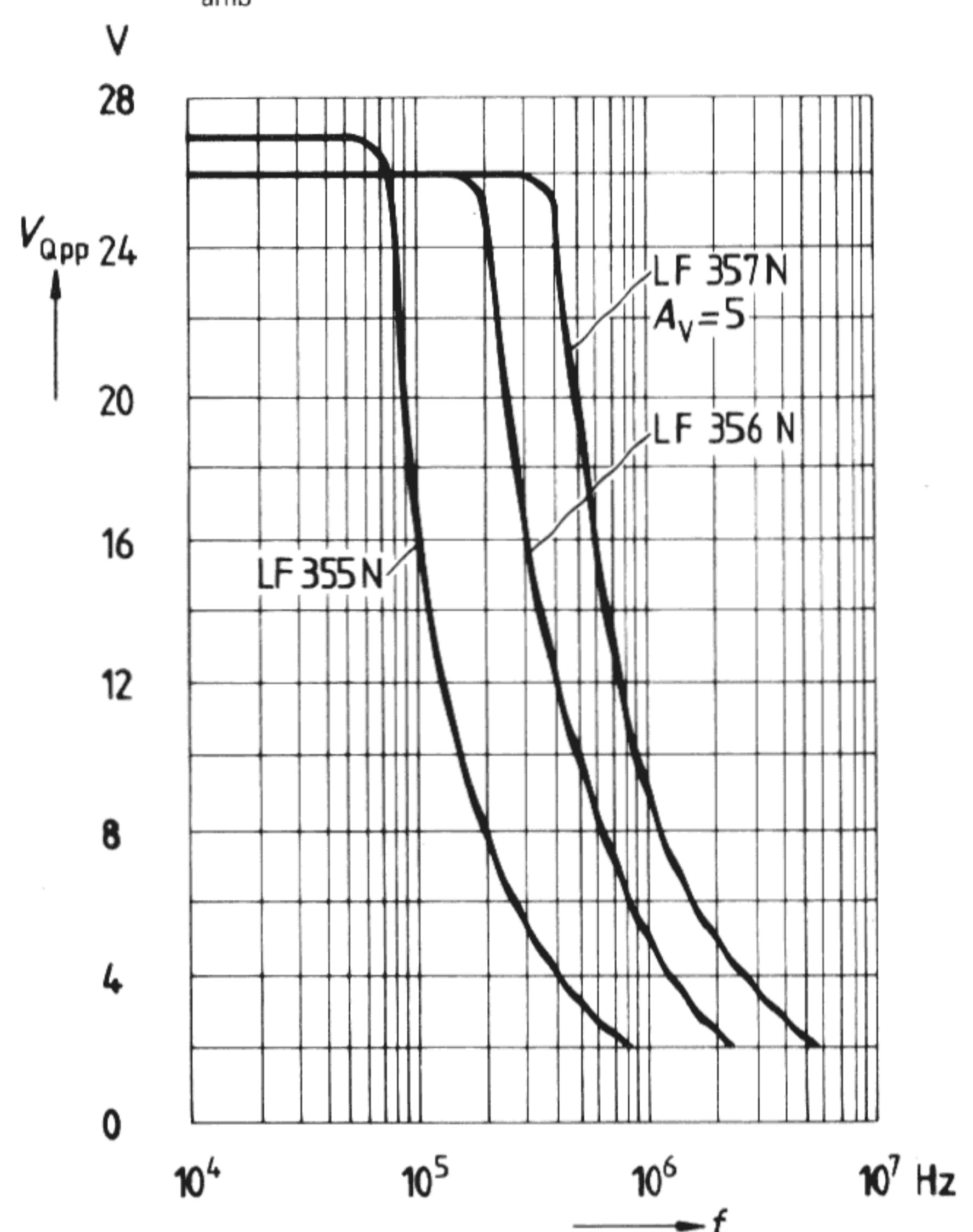
Supply voltage rejection

$k_{SVR} = f(f)$
 $V_S = \pm 15 \text{ V}, T_{\text{amb}} = 25^\circ\text{C}$



Output voltage versus frequency

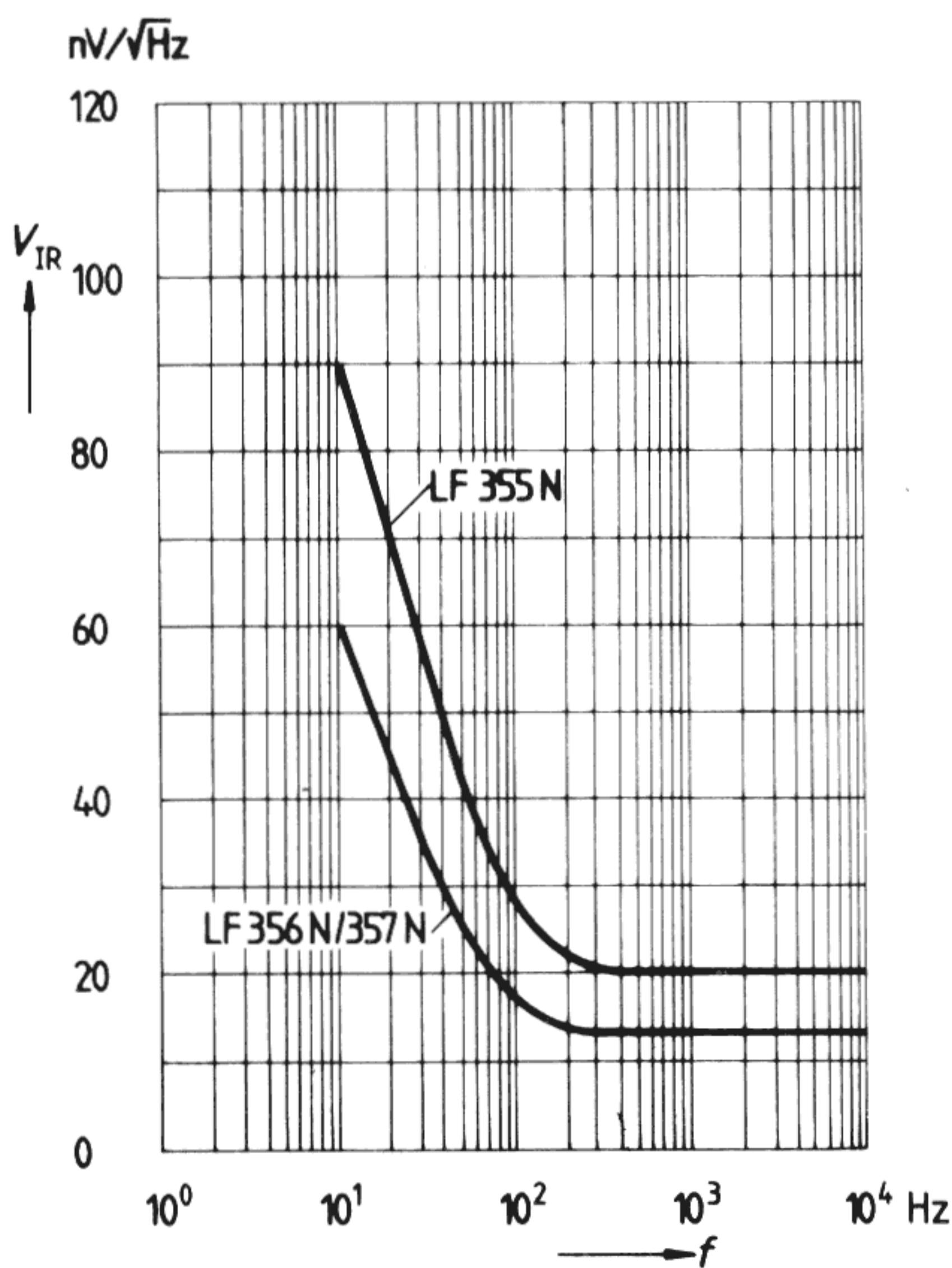
$V_{QPP} = f(f); R_L = 2 \text{ k}\Omega, A_V = 1$
 Distortion factor <1% $V_S = \pm 15 \text{ V}, T_{\text{amb}} = 25^\circ\text{C}$



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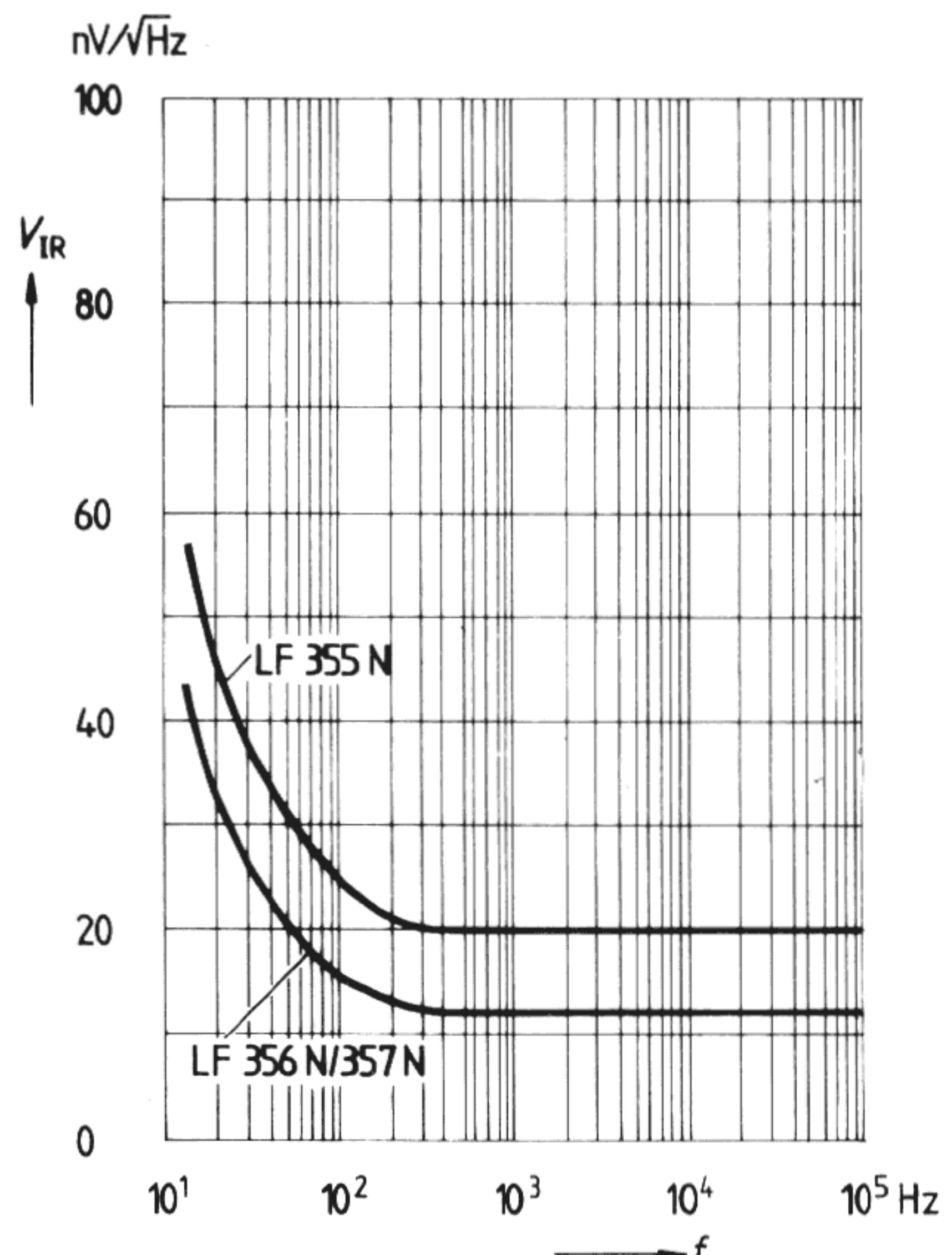
Input noise voltage versus frequency

$V_{IN} = f(f)$
 $V_S = \pm 15 \text{ V}, T_{\text{amb}} = 25^\circ\text{C}$

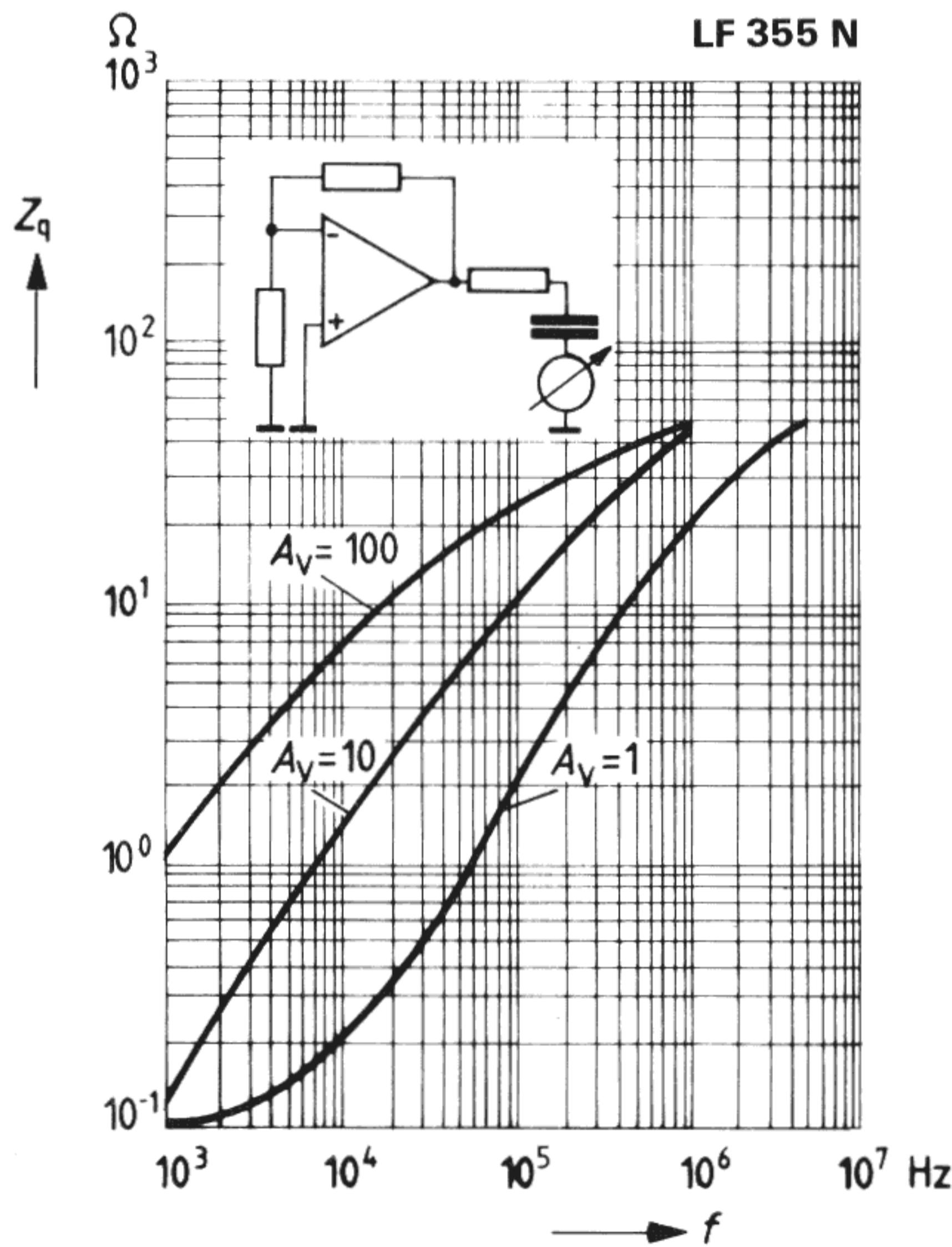


Input noise voltage versus frequency

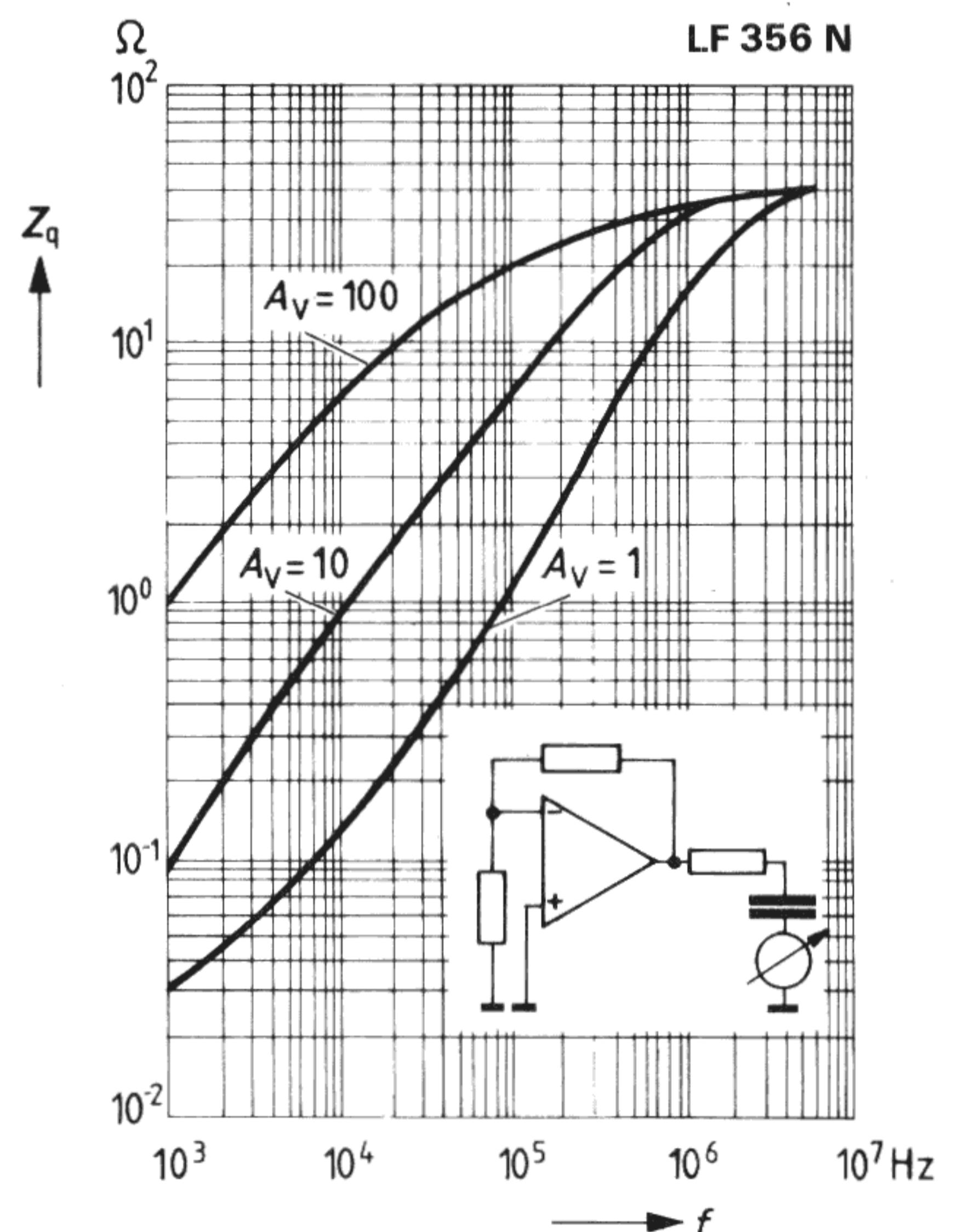
$V_{IN} = f(f)$
 $V_S = \pm 15 \text{ V}, T_{\text{amb}} = 25^\circ\text{C}$



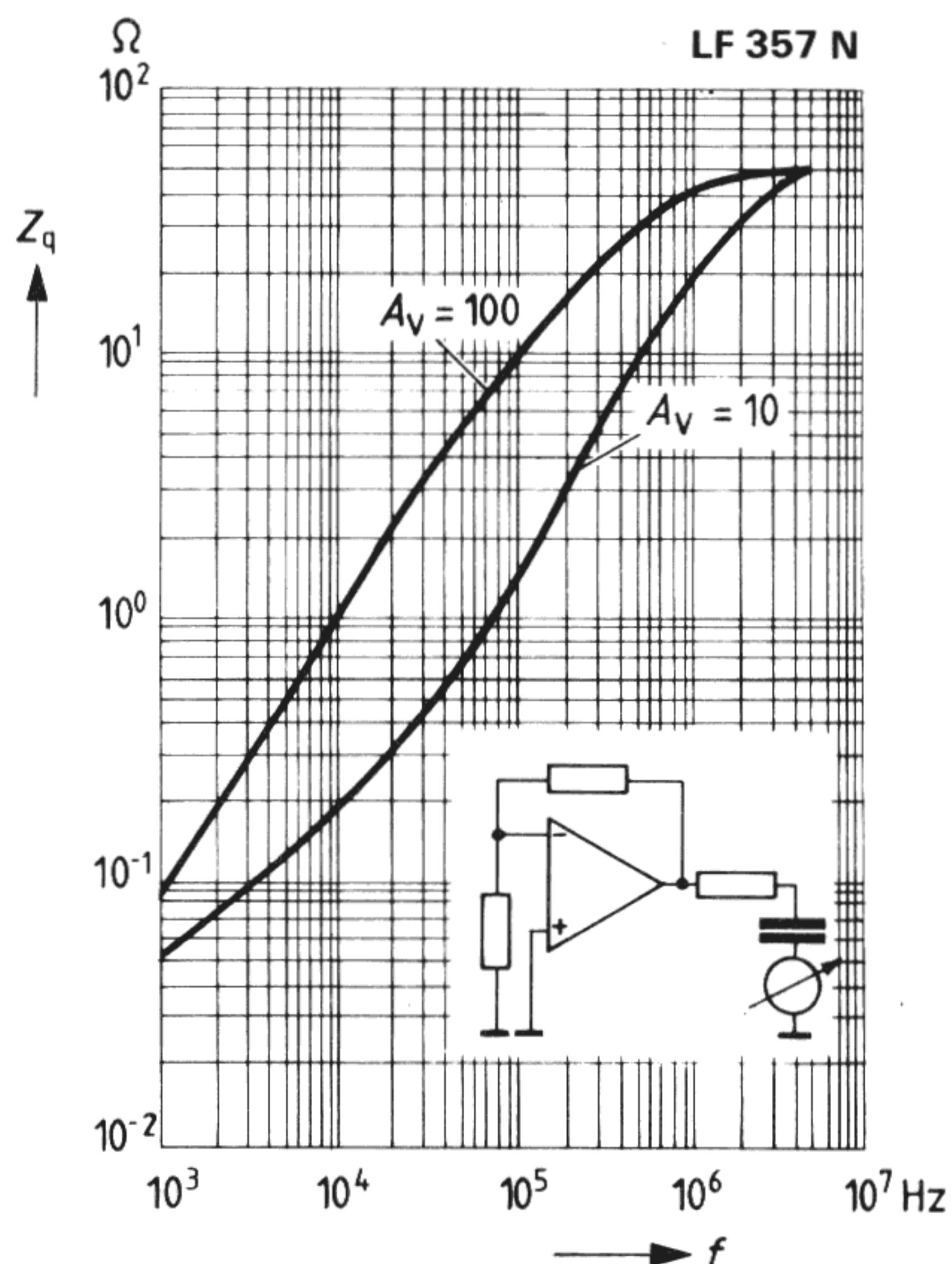
Output impedance $Z_q = f(f)$
 $V_S = \pm 15 \text{ V}$, $T_{\text{amb}} = 25^\circ\text{C}$

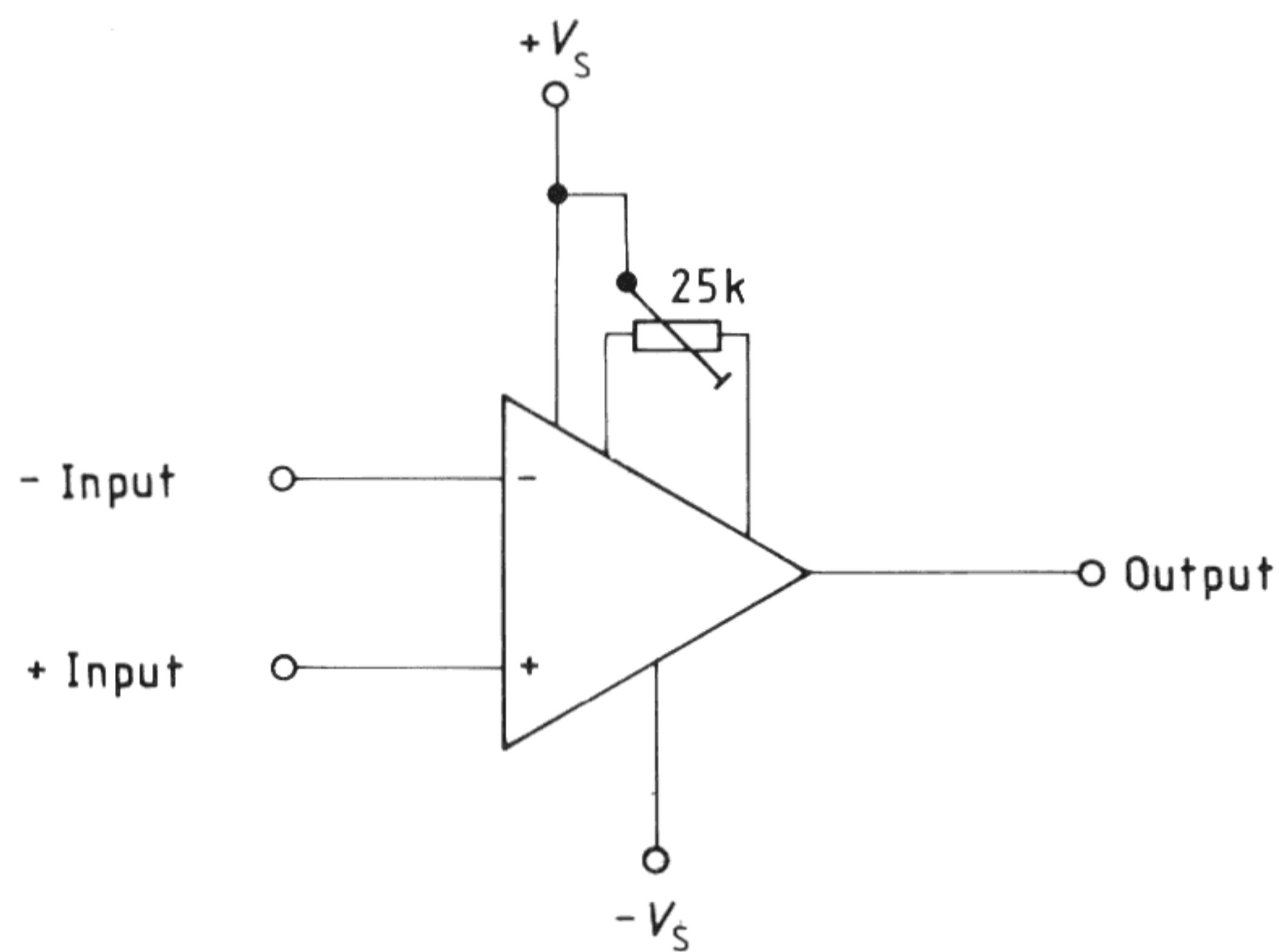


Output impedance $Z_q = f(f)$
 $V_S = \pm 15 \text{ V}$, $T_{\text{amb}} = 25^\circ\text{C}$

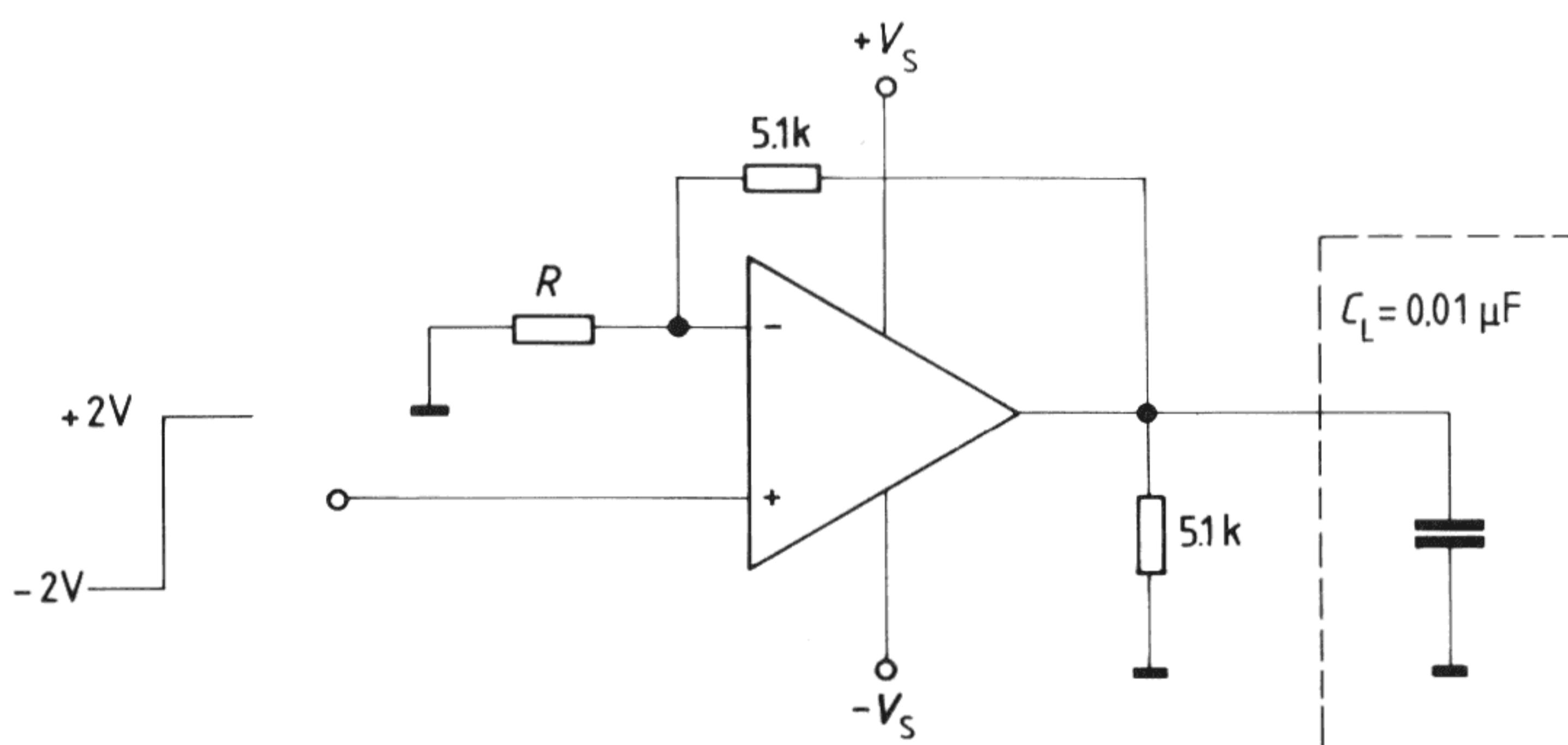


Output impedance $Z_q = f(f)$
 $V_S = \pm 15 \text{ V}$, $T_{\text{amb}} = 25^\circ\text{C}$



Hints for application**1. Offset voltage compensation**

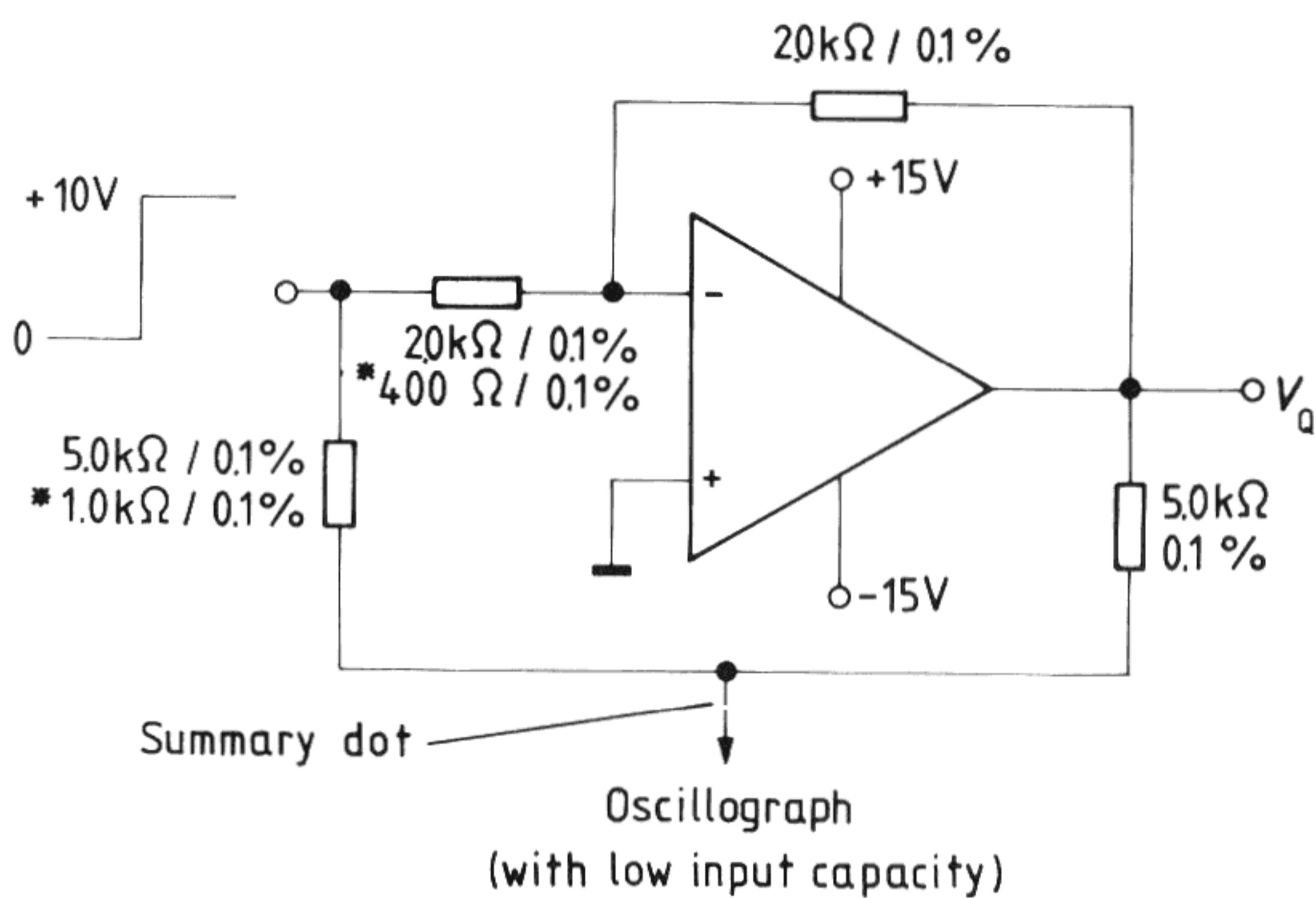
The input offset voltage is compensated with a 25 k potentiometer. The potentiometer wiper is connected to positive supply voltage +V_S.

2. Capacitive output load

R = 5.1 k for LF 355 N/LF 356 N
R = 1.3 k for LF 357

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Provided the stability remains constant, high capacitances can be loaded by amplifiers with $A_V = 1$. $C_{L\max} \geq 0.01 \mu F$, overshoot $\leq 20\%$, transient time $\approx 5 \mu s$.

3. Circuit for transient time measurements

*for $A_V = 5$ of the LF 357 N.

The transient time for the LF 355 N/LF 356 N is measured with $A_V = 1$, and for the LF 357 N with $A_V = 5$.